Direct Methanol Anion Exchange Membrane Fuel Cell with a Non-Platinum Group Metal Cathode based on Iron-Aminoantipyrine Catalyst

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Abstract

The objective of the current report is to compare the performance of poly(phenylene) based anion exchange membranes in an alkaline direct methanol fuel cell when platinum cathode catalysts are replaced with non-platinum cathode catalysts. In a KOH-free methanol fuel, we show that a less expensive non-Pt cathode catalyst (derived from Fe-Aminoantipyrine, Fe-AAPyr, using Generations 1 and 2 sacrificial silica supports) provide better or comparable performance to commercial Pt cathode catalysts. The peak power density, current density and open circuit voltage of Fe-AAPyr-G-1 in 1M methanol at 80 °C are 2.78 mW cm$^{-2}$, 19.1 mA cm$^{-2}$ and 0.7 V respectively. In a direct methanol fuel cell utilizing KOH in the fuel feed, the non-Pt catalyst shows promising peak power density of 52 mW cm$^{-2}$ with the Fe-AAPyr-G-2 cathode catalyst, comparable to a commercial Pt catalyst.

Keywords: Oxygen Reduction Reaction, Anion Exchange Membrane, Fuel Cell, Direct Methanol Fuel Cell, non-Platinum Group Metal Catalyst
1. Introduction

Alkaline fuel cells (AFCs) have the advantage over proton exchange membrane (PEM) fuel cells in that there is the possibility of using non-precious metal catalysts for both the oxygen reduction reaction and for fuel oxidation [1]. The recent advances in anion exchange membranes (AEMs) in terms of chemical durability and mechanical robustness has led to the development of fuel cells based on AEMs that have much higher system power densities than liquid electrolyte based AFCs [2-7]. Direct methanol AEM fuel cells (DMAEMFCs) have advantages over the equivalent PEM based fuel cells that include, simpler water management, lower methanol permeability, and the use of non- platinum metal catalysts [1, 8]. All fuel cells run with this technology to date that show higher power densities use added OH⁻ ions in the fuel. The ultimate aim would be to run these direct methanol fuel cells without added KOH [9]. The reason for adding hydroxide is that stoichiometrically the oxidation of methanol requires 6 OH⁻ ions, the hydroxide flushes the slow moving carbonate and bicarbonate, formed from reaction of CO₂ and OH⁻, out of the anode and it improves the anode potential as > 300 mV reduction in anode over potential is possible [5]. Comparison of DMAEMFCs with and without added KOH is useful as it sets a reference point with other reports and the chemical degradation of the MEA with added hydroxide especially at higher temperatures is much faster. The use of KOH has been reported with fuel cells using commercial AEMs such as the Tokuyama membrane, Fumatech FAA-2, and Morgane ADP by companies such as the Diahatsu Motor Company [10-16].

The most attractive feature of alkaline fuel cells is the use of non-Pt metal catalysts as they can operate with high stability and activity in alkaline media when compared to acidic media. In addition, this can also reduce the cost of fabricating fuel cell electrodes, CO poisoning, and the slow cathode reaction kinetics observed for platinum catalyst [17, 18]. The methanol tolerance of non-Pt catalysts on the cathode would also reduce the voltage loss due to mixed potentials that is seen while methanol cross-over occurs to the cathode. The possible non-Pt cathode materials are reviewed in literature [19]. Non-Pt catalysts in alkaline fuel cells have been demonstrated to perform well with fuels such as hydrogen, methanol, and ethanol [20-27]. The motivation of alkaline direct methanol fuel cell (ADMFC) researchers is to develop non-Pt catalysts for both anode and cathode that in combination with AEMs exhibit high performance and long durability.
Our previous work was focused on detailed study of two AEMs (ATMPP and TMAC6PP, both 2.4 meq/g), developed by Sandia National Laboratories in an alkaline direct methanol fuel cell [9]. ATMPP and TMAC6PP are poly(phenylene) based AEMs with benzyltrimethylammonium (ATM) cation and trimethyl ammonium cation with a hexamethylene spacer (TMAC6) respectively (Figure 1). The ionomers TMAC6PPC6l and TMAC6PPC6h, Figure 1, using a hexamethylene chain introduced into the backbone to make the polymer more rubbery and soluble in organic solvents were developed in low and high IEC, 2.13 meq g\(^{-1}\) and 2.60 meq g\(^{-1}\) respectively. TMAC6PPC6h with a higher water uptake designed to increase the hydrophilicity of the anode thereby enhancing the diffusion of aqueous electrolyte and methanol; whereas the low water uptake TMAC6PPC6l was designed to reduce the flooding on the cathode [28]. Synthesis and properties of the ionomer such as water uptake and conductivity have been reported by one of the authors elsewhere [29-32]. The properties of these AEMs were demonstrated to be potential for fuel cell applications [29-31]. Furthermore, some of us, Atanassov et al. have demonstrated the application of the poly(phenylene) ionomer for electrocatalysis and H\(_2\)-O\(_2\) fuel cells [33-35].

This paper is a logical extension of our previous work on application of these AEMs for DMAEMFCs with commercial platinum catalysts on both electrodes [9]. The study compared the performance of the AEMs with different catalysts and GDLs. As the details can be found elsewhere, here we summarize the results for the reader’s better understanding. A comparison of the fuel cell performances in KOH free 1M methanol of the two AEMs, ATMPP and TMAC6PP with identical MEA components (both had a commercial 50 % Pt on high surface area carbon catalyst) showed a slightly better performance for the TMAC6PP MEA over ATMPP MEA. TMAC6PP MEA demonstrated peak power and current densities of 3.6 mW cm\(^{-2}\) and 26.7 mA cm\(^{-2}\) while ATMPP MEA showed 3.1 mW cm\(^{-2}\) and 26.0 mA cm\(^{-2}\) at 80 °C, 100 % RH. This slight improvement of TMAC6PP MEA could be related to the relatively better stability of TMAC6PP over ATMPP. This agrees with the results demonstrated by Hibbs that showed only 5% decrease in conductivity for TMAC6PP as opposed to 33 % decrement for ATMPP after they were soaked in 4M KOH for 14 days [29]. As the AEMs are new and the interfacial chemistries between catalysts have not been studied before, we investigated AEM-Catalyst combinations of the ATMPP with both commercial catalysts. The current densities of ATMPP-Etek and ATMPP-50%Pt/C MEAs were 7.2 and 26.0 mA cm\(^{-2}\) respectively. The power densities of ATMPP-Etek
and ATMPP-50%Pt/C MEAs were 3.1 and 0.85 mW cm$^{-2}$ respectively. The key factors to enhance the performance was achieved by improving the hydrophilicity and hydrophobicity of the anode and cathode respectively. As we have compared the performances of AEMs in our previous work, the current report does not intend to compare these two AEMs.

The objective of the current report is to study the performance of alkaline direct methanol fuel cell using poly(phenylene) based anion exchange membranes when platinum cathode catalysts are replaced with non-platinum cathode catalysts prepared by some of the authors [36-40]. To achieve this, we studied TMAC6PP based MEAs with noble metal catalyst (commercial 50%Pt/C, MEA-4) and non- noble metal catalyst, Fe-AAPyr-G2 (MEA-3). Similarly, ATMPP based MEAs were studied with and without noble metal cathode catalyst, MEA-2 and MEA-1 respectively. This now represents one of the first fuel cell investigations on non-platinum cathode catalysts reported, as most previous studies only report ORR activity in an aqueous half-cell [41, 42].

2. Experimental

2.1 Materials

The platinum catalysts, 20% Pt on Vulcan XC-72 and 50 % Pt on high surface area carbon were purchased from E-TEK, Inc. and a commercial supplier respectively. Gas diffusion layers were a hydrophobic carbon cloth GDL, GDL LT 1400-W, from E-TEK, Inc. and a hydrophilic carbonized woven fiber fabric, Panex® 30, from Zoltek. The AEMs, ATMPP and TMAC6PP, and ionomers, TMAC6PPC6l and TMAC6PPC6h, were prepared as reported previously [29, 30]. Fe-AAPyr catalysts were prepared by wet impregnation of iron and aminoantipyrine precursors (Sigma Aldrich) onto the surface of two different silicas, Generation-1: Cab-O-Sil™ EH-5, surface area: ~400 m$^2$ g$^{-1}$ and Generation-2: Cab-O-Sil™ M-5, surface area: ~225 m$^2$ g$^{-1}$, designated Fe-AAPyr-G1 and Fe-AAPyr-G2 respectively. First, a calculated amount of silica (the total metal loading on silica was calculated as ~20wt.%) was dispersed in a mixture of water and acetone (1:1 by volume) in an ultrasound bath. Then, a solution of aminoantipyrine in acetone was added to silica and ultrasonicated for 40 min. Finally, a solution of iron nitrate (Fe(NO$_3$)$_3$.9H$_2$O) was added to SiO$_2$-AAPyr solution and ultrasonicated for 8 h. After ultrasonic treatment viscous gel of silica and Fe-AAPyr was dried overnight at T=85 °C. The obtained solid
was ground to a fine powder, and then subjected heat treatment (HT). The general conditions of HT were UHP nitrogen (flow rate 100 cc min\(^{-1}\)), 10 deg min\(^{-1}\) temperature ramp rate, and a 1 h pyrolyzation time at T= 900 °C. The sacrificial support was removed by means of 20 wt.% of HF. The obtained wet powder was washed by DI water until pH≈5 and dried at T= 45°C.

2.2 Characterization
The catalysts were characterized by Brunauer-Emmet-Teller (BET) measurements, SEM (Hitachi S-5200) and TEM (JEOL 2010 EX HREM).

2.3 Ring Disk Electrode
Electrochemical analysis for synthesized catalysts was performed using the Pine Instrument Company electrochemical analysis system. The rotational speed was 1200RPM, with a scan rate of 5 mV sec\(^{-1}\). The electrolyte was 1M KOH saturated in O\(_2\) at room temperature. A platinum wire counter electrode, and Hg/HgO were used. Working electrodes were prepared by mixing 5 mg of the Fe-AAPyr electrocatalyst with 850 μL of isopropyl alcohol, and 150 μL of Nafion\(^\circledR\) (0.5% wt., DuPont). The mixture was sonicated before 30 μL was applied onto a glassy carbon disk with a sectional area of 0.2474 cm\(^2\). The loading of catalyst on the electrode was 0.6 mg cm\(^{-2}\).

2.4 Membrane Electrode Assembly (MEA)

Table 1 details the components of MEAs studied in this paper. MEAs were fabricated with commercial 20 % Pt/C, E-TEK (MEA-1 and MEA-2) and 50 % Pt/C (MEA-3 and 4) as anode catalysts. Fe-AAPyr-G-1 and Fe-AAPyr-G-2 are the cathode catalysts used in MEA-1 and MEA-3. To compare the performance of non-Pt cathode catalysts (MEA-1 and MEA-3), control MEAs (MEA-2 and MEA-4) were fabricated with the two commercial catalysts. In general, catalyst inks were made by mixing catalyst, DI water, isopropanol and ATMPP or TMAC6PPC6l (IEC: 2.13 meq/g) and TMAC6PPC6h (IEC: 2.60 meq/g) (3% solution in methanol) with a catalyst to ionomer mass ratio of 4:1. Catalyst inks were painted on 5.48 cm\(^2\) gas diffusion layers to obtain a loading of 1.4 mg of Pt cm\(^{-2}\) with an ETEK catalyst, 2.5 mg of Pt cm\(^{-2}\) with the commercial catalyst and 5.48 mg cm\(^{-2}\) of Fe-AAPyr-G-1 and Fe-AAPyr-G-2 catalyst. The electrodes were hot pressed on ATMPP or TMAC6PP membranes using a digital combo multi-purpose press,
DC14, Geo Knight & Co. Inc. at 66 °C and 80 psig for 90s. Prior to any tests, MEAs were soaked in 1M NaOH for 2 h to convert the membrane from the Br⁻ form to OH⁻ form. Following this, MEAs were subsequently soaked in water with frequent changes of water to ensure complete removal of NaOH and to obtain a neutral pH.

2.5 Fuel Cell Testing

Single cell hardware from Fuel Cell technologies, Inc. with a working area of 5.48 cm² and single serpentine flow fields was used. The supplied anodized aluminum endplates were replaced with stainless steel end plates to withstand the alkaline conditions. The effluent from the fuel cell reaches the back-pressure regulators, followed by a water trap which separates out any condensed liquid in the exit lines. An isocratic HPLC pump (Chromtech) was used to pump the methanol solution or methanol in KOH solution to the anode. Oxygen was fed to the cathode through a modular gas handling/gas metering system (Lynntech Industry, Inc.) through a humidity bottle maintained at 80 °C. The purge gas N₂ and flow rate of O₂ was controlled using FC power software (Lynntech Industry, Inc.). The fuel and oxygen flow rates were set to 0.5 ml min⁻¹ and 0.2 L min⁻¹ respectively in this study. The cell temperature was controlled at 80 °C. A MSTAT4+ multi-potentiostat (Arbin Instruments) was used to conduct polarization experiments. The polarization curves were obtained by stepping down the potential from open circuit potential until the limiting current is achieved. In situ impedance spectra were measured potentiostatically at different potentials on the polarization curve using a Gamry Instruments potentiostat. The frequencies were varied between 100,000 and 0.1 Hz with the data points being 10 per decade. The AC voltage was 10 mV root mean squared.

3. Results and Discussion

3.1 Catalyst Characterization

The catalysts were prepared via the sacrificial support method (SSM) [36-40]. The morphology of the catalysts is shown in Figure 2. It can be seen in the SEM and TEM images of Fe-AAPyr-G1 materials that the catalyst consists of a well-developed porous matrix (Figure 2 a, b). The analysis of the SEM and TEM images revealed that material has at least bi-modal pore size distribution: smaller pores in the range of 20-40 nm and larger pores with diameter >100nm. Based on the empirical observation from our previous works smaller pores can be related to
decomposition of organic precursor while larger pores are formed after silica support removal. The ratio between silica and organic precursor as well as a nature of sacrificial support allows the controlling final morphology of catalysts. It should be mentioned that due to the fact that these catalysts are fabricated by the sacrificial support method that does not utilize artificially added carbon (in contrast to conventional methods) the density of active sites in open-frame structure is significantly higher compared with traditional catalysts[39]. The surface area of both materials is 650 m²/g. It is well-known fact that presence of Fe²⁺/Fe³⁺ pairs can result in formation of radical and fast degradation of anion-exchange membrane. The TEM images were collected in multiple spots of catalysts in order to determine the presence of residual iron nano-particles. Such nano-particles were not observed which can be expected taking into account aggressive leaching step with HF acid.

In order to evaluate influence of heat treatment parameters of the catalysts, such as temperature and duration of the pyrolysis, we prepared 4 different catalysts. Those materials were screened in Rotating Disk Electrode experiment in 1M KOH, saturated with O₂, Figure 3. The results are compared to the commercial Pt catalyst and as can be seen in the Figure the Fe containing catalysts all outperform the Pt containing catalyst in base. It was found that Fe-AAPyr-G1 synthesized at T = 900 °C and t = 1h had the highest activity and so this material was down-selected for further MEA tests in the fuel cell.

3.2 Direct Methanol Fuel cell without KOH

Here we compare the data for the Fe containing cathode electrodes to the Pt baselining studies of our previous report [9]. The data for all of the MEAs is shown in Figure 4 at 80 °C, 100 % RH using 1M methanol. The fuel cell performances of both the non-Pt cathode catalysts (Fe-AAPyr-G1 and Fe-AAPyr-G2) are compared to commercial Pt cathode catalysts from Etek (20% Pt/C) and the other commercial supplier (50% Pt/C). We were able to operate the fuel cell at 80 °C and collect steady state data as these membranes have good chemical stability. AEM Fuel cells are usually operated at 60 °C as many cationic ammonium groups decompose above this temperature under fuel cell operation. The elevated temperature enables carbonate decomposition in the anode, improves the electrode kinetics, and reduces the thermodynamic voltage losses [6, 25]. It can be seen Fe-AAPyr-G1 cathode (MEA-1) outperformed the commercial cathode (MEA-2) in terms of open circuit voltage (OCV), power and current densities (Table 2). MEA-1 (0.7 V)
shows 240 mV higher OCV than the MEA-2 (0.46 V), indicating less of the methanol that crossed over the membrane reacted with the non-Pt cathode catalyst. The maximum current densities of MEA-1 and 2 were 19.1 and 7.2 mA cm\(^2\); the peak power densities being 2.78 and 0.85 for MEA-1 and 2 respectively. The normalized current density at 0.1 V was comparable on a mass basis for both catalysts, which is significant considering the very high market price of Pt as compared to Fe. All other components of the MEAs being identical, the enhanced performance of MEA-1 can be attributed to the Fe-N-C catalyst.

Polarization curves measured for Fe-AAPyr-G2 cathode (MEA-3) and its control MEA-4 with the commercial Pt cathode catalyst demonstrated 120 mV higher OCV for the Fe-AAPyr-G2 catalyst indicating better methanol tolerance (Figure 4). These systems use the more chemically stable TMAC6PP membrane, derivative ionomers, the commercial Pt catalyst and Zoltek hydrophilic GDL in the anode. Nevertheless, the commercial Pt catalyst achieved higher current and power densities than the non-Pt catalyst. At low current density region, until 1.35 mA cm\(^2\), there is not much difference in their performances, implying the same kinetic losses of the catalyst systems in the electrode. When a higher current is drawn from the cell, MEA-3 showed an increased ohmic drop, voltage dropped rapidly to reach a maximum current density of 9.8 mA cm\(^2\). MEA-4 showed a lesser ohmic loss, a steady drop in the voltage upon high current draw was observed to reach a maximum current density of 29.5 mA cm\(^2\), which is three times higher than for the non-Pt catalyst. This implies that the long chain TMAC6PP6l ionomer interacts less well in terms of ionic conductivity with the Fe-AAPyr-G2 catalyst than it does with the Pt catalyst. The poor compatibility of Fe-AAPyr-TMAC6PPC6l interface could have been due to a relatively higher degree of swelling and de-swelling of the ionomer resulting in a poor performance. To ensure this, in depth investigations of the transport properties of TMAC6PPC6l are required. The poor catalyst binder interaction is also evident from a rapid voltage drop with significant ohmic loss. To elucidate the ohmic loss difference between the two MEAs, impedance spectra of the MEAs were measured during fuel cell operation at 400 mV (Figure 5). Ohmic resistance which is the high frequency intercept (x-axis intercept), were 50 mΩ cm\(^2\) and 27 mΩ cm\(^2\) for MEA-3 and MEA-4 respectively [20, 25, 43]. Ohmic resistance has resulted from the cathode catalyst and its interaction with the ionomer as all other components of the MEAs remain the same. The power density achieved by the MEA-4 (3.97 mW cm\(^2\)) is 2.8 times higher than the MEA-3 (1.40 mW cm\(^2\)). The maximum power density achieved for the Fe-
AAPyr-G2 cathode catalyst MEA is only half that of the Pt cathode MEA, which is significant when one considers the raw materials costs.

### 3.3 Direct Methanol fuel cell with added KOH

In the presence of KOH, ATMPP Fe-AAPyr-G1 based MEAs-1 and its Pt-control MEA-2 demonstrated enhanced performance (Figure 6). As shown in the literature, the enhancement could be due to adequate supply of OH⁻ ions required for methanol oxidation and reduced anode over potential [44]. The performance of MEA-1 was superior both in the presence and absence of KOH when compared to MEA-2, but still lower than the systems with the TMAC6PP membrane, the commercial Pt catalyst and Zoltek anode GDL. MEA-2 had a 0.93 V OCV, which is 100 mV higher than the MEA-1 (0.83 V). The low current slope of MEA-1s polarization curve is also much steeper than for the Pt cathode, implying that the non-precious catalyst does not do as well kinetically. Significant ohmic loss was observed in the Pt-catalyzed cathode, MEA-2, and the voltage dropped rapidly from the OCV when high current was drawn from the cell and was inoperable below, 0.35 V, suggesting significant issues with the ATMPP ionomer and Pt catalyst. In comparison to the control, the non-Pt catalyst performed much better in terms of ohmic losses, the voltage drop was steady when a higher current was drawn. A maximum current density of 117 mA cm⁻² was achieved which is 2.3 times higher than MEA-2 which reached a maximum of 50.7 mA cm⁻². The corresponding peak power densities of MEA-1 and MEA-2 were 17.7 and 24.7 mW cm⁻² respectively.

In our previous study using Pt on both sides of the MEA, we showed that the best performance was with the commercial Pt catalyst, the long chain cationic membrane, TMAC6PP with TMAC6PPC6 ionomers, and the Zoltek hydrophilic GDL on the anode [9]. We also demonstrated the effect of varying MeOH and KOH concentration. In the presence of KOH, MEA-3 also showed significant improvement in the performance and the comparable data is shown in, Figure 7. The open circuit potentials at all concentrations were very close, ~ 0.88 V (Table 3) [21]. This fact shows that the Fe based catalyst shows excellent tolerance towards MeOH oxidation as the OCV is invariant with MeOH concentration, and if it reacted with the MeOH would fall with increasing MeOH concentration. The maximum current density and peak power density for the baseline, 1M methanol and 1M KOH were 167.78 mA cm⁻² and 44.2 mW cm⁻² respectively. When either the electrolyte or KOH concentration was increased to 2M, the
performances were found to improve when compared to the baseline 1M-1M concentrations, the maximum current density and peak power density increased up to 182.5 mA cm$^{-2}$ and 47.6 mW cm$^{-2}$ respectively for 1M-2M concentration and these values were 217.9 mA cm$^{-2}$ and 47.5 mW cm$^{-2}$ for 2M-1M concentration. When both fuel and electrolyte concentrations were increased to 2M, the best performance was observed, with a maximum current density of 234.3 5 mA cm$^{-2}$ and 51.97 mW cm$^{-2}$ respectively. A further raise of fuel and KOH concentration to 3M, reduced the current density and power density to 229 mA cm$^{-2}$ and 45.9 mW cm$^{-2}$ respectively. The Pt cathode catalyst system showed the best performance at 1M MeOH and 1M KOH, 226 mA cm$^{-2}$ current density and 53.4 mW cm$^{-2}$ power density [9]. So in KOH the non-precious Fe-AAPyr-G2 catalyst has the same performance as the Pt-catalyst on the cathode, demonstrating that non-precious catalyst are indeed practical in AEM fuel cells and also offer the possibility of MeOH tolerance, negating the effects of MeOH crossover through the membrane.

The performance comparison between Figures 3 and 4 demonstrate that the replacement of non-Pt cathode catalyst did not compromise the performance. This performance of the non-Pt catalyst is better than the power density observed from many MEAs with commercial AEMs and Pt catalysts in the presence of KOH. With a Morgane ADP from Solvay and Pt catalysts, power densities between 6 and 10 mW cm$^{-2}$ are reported [12]. Similarly, with a Tokuyama membrane and a Pt catalysts a peak power density of 12.8 mW cm$^{-2}$ was observed in 7M methanol and 1M KOH [14].

4. Conclusions

This work reports the study of non-platinum cathode catalysts with poly(phenylene) based AEMs, ATMPP and TMAC6PP for direct methanol alkaline fuel cells. In the absence of KOH both the Fe-AAPyr-G1 and Fe-AAPyr-G2 catalysts gave much higher OCVs when used as the catalyst I the cathode than Pt, due to their superior ability to resist MeOH oxidation. The Fe-AAPyr-G1 cathode catalyst with ATMPP membrane outperformed the platinum catalyst (Etek) in KOH free methanol showing remarkably three times enhancement in power density. The enhanced performance of Fe-AAPyr-G-1 in terms of OCV, power and current densities was attributed to the non-platinum cathode catalyst. Nevertheless, the performance of Fe-AAPyr-G-2 was not as significant (~ 2.8 times low power density) and was lower than the commercial Pt catalyst with a TMAC6PP. This is attributed to the poorer compatibility of the TMAC6PPC6
ionomer with the Fe based catalyst. Nevertheless, both catalysts performance is significant when precious metal material costs are factored.

The OCV advantage of the Fe based catalysts versus the Pt based catalysts was not as significant when the MeOH fuel was co-fed with KOH. Investigation of the activities in KOH demonstrated better performance for Fe-AAPyr-G1 when compared to the Etek Pt catalyst in the ATMPP system, showing ~1.4 times higher power density. When using the Fe-AAPyr-G2 and the commercial Pt catalyst in KOH in the TMAC6PPC6 system the same high current densities could be achieved for both Fe based and Pt based catalysts, although the optimum performance for the Fe based system was at 2M concentration for both MeOH and KOH. This study shows that the Fe-AAPyr catalyst can replace Pt catalysts in the cathode of direct MeOH fuel cells using AEMs and that these catalysts may be tuned to have even superior performance.

Acknowledgments

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References


Table 1. Membrane Electrode Assemblies and their components

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<thead>
<tr>
<th>MEA</th>
<th>Anode Catalyst</th>
<th>Anode GDL</th>
<th>Anode Ionomer</th>
<th>Cathode</th>
<th>Cathode GDL</th>
<th>Cathode Ionomer</th>
<th>AEM</th>
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<tr>
<td>MEA-1</td>
<td>Pt/C, Etek</td>
<td>Etek</td>
<td>ATMPP</td>
<td>Fe-AAPyr-G1</td>
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<td>ATMPP</td>
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<td>MEA-2</td>
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<td>ATMPP</td>
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<td>Etek</td>
<td>ATMPP</td>
<td>ATMPP</td>
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<td>TMAC6PPC6h</td>
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<td>Etek</td>
<td>TMAC6PPC6l</td>
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<td>Pt/C, 50%Pt/C</td>
<td>Etek</td>
<td>TMAC6PPC6l</td>
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Table 2. Fuel cell performance data in 1M Methanol at 80 °C, 100% RH

<table>
<thead>
<tr>
<th>MEA</th>
<th>OCP (V)</th>
<th>Current density at 0.1 V (mA cm$^{-2}$)</th>
<th>Current density at 0.1 V (mA cm$^{-2}$ mgPt$^{-1}$ or mg(Fe-N-C)$^{-1}$)**</th>
<th>Peak Power density (mW cm$^{-2}$)</th>
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<tr>
<td>MEA-1</td>
<td>0.7</td>
<td>19.1 (at 0.15 V)</td>
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<td>MEA-2 [9]</td>
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<td>MEA-3</td>
<td>0.68</td>
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<td>MEA-4 [9]</td>
<td>0.56</td>
<td>29.5</td>
<td>11.5</td>
<td>3.97</td>
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Table 3. DMAFC results as a function of concentrations of methanol and KOH at 80 °C, 100% RH

<table>
<thead>
<tr>
<th>MeOH - KOH</th>
<th>MEA-3</th>
<th>MEA-4 [9]</th>
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<tr>
<td></td>
<td>OCP</td>
<td>Current density</td>
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<td></td>
<td>(V)</td>
<td>(mA cm(^{-2}))</td>
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<tr>
<td>1M – 1M</td>
<td>0.89</td>
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<td>3M – 3M</td>
<td>0.88</td>
<td>229.7</td>
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</tbody>
</table>

** - Experiment not performed at this condition
Figure 1. Structure of the polymers used in membranes and as ionomers in electrodes
Figure 2. Images of best performing Fe-AAPyr-G1: a) SEM and b) TEM
Figure 3. Electrochemical data for Fe-AAPyr-G1 catalysts with variation of heat treatment parameters in comparison with commercial 50wt% Pt/C: T=950 °C, t=1h (▬▬), T=950 °C, t=2h (▬ ▬), T=900 °C, t=1h (• • • •) and T=900 °C, t=2h (▬▬▬), commercial 50wt% Pt/C (▬ ▲ ▬). Conditions: 1 M KOH saturated with O₂, 1200RPM, 5 mV s⁻¹, catalyst loading 0.6mg cm⁻².
Figure 4. DMAFC performances of MEA-1 (Diamonds), MEA-2 (Circles) [9], MEA-3 (Squares), MEA-4 (Triangles) [9] in 1M methanol at 80 °C, 100% RH, polarization curves (open symbols), power curves (closed symbols).
Figure 5. Impedance spectra of MEA-3 (—) and MEA-4 (-----) [9] in 1M methanol at 400 mV, fuel cell operated at 80 °C, 100 % RH
Figure 6. DMAFC performances of non-Pt cathode catalyst (MEA-1, circles) against a Pt cathode catalyst (MEA-2, triangles) [9] in 1M methanol and 1M KOH at 80 °C, 100% RH.
Figure 7. DMAFC performances of MEA-3 with UNM G-2 cathode catalyst as a function of fuel-electrolyte concentrations (solid diamonds- 1M-1M; triangles-2M-1M; circles- 1M-2M; open diamonds-2M-2M; squares- 3M-3M)