Mechanisms of Radiation-Induced Segregation in CrFeCoNi-based Single-Phase Concentrated Solid Solution Alloys

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ABSTRACT

Single-phase concentrated solid solution alloys have attracted wide interest due to their superior mechanical properties and enhanced radiation tolerance, which make them promising candidates for the structural applications in next-generation nuclear reactors. However, little has been understood about the intrinsic stability of their as-synthesized high-entropy configurations against radiation damage. Here we report the element segregation in CrFeCoNi, CrFeCoNiMn, and CrFeCoNiPd equiatomic alloys when subjected to 1250 kV electron irradiations at 400 °C up to a damage level of 1 displacement per atom. Cr/Fe/Mn/Pd can deplete and Co/Ni can accumulate at radiation-induced dislocation loops, while the actively segregating elements are alloy-specific. Moreover, electron-irradiated matrix of CrFeCoNiMn and CrFeCoNiPd shows $L1_0$ (NiMn)-type ordering decomposition and $\langle 001 \rangle$ -oriented spinodal decomposition between Co/Ni and Pd, respectively. These findings are rationalized based on the atomic size difference and enthalpy of mixing between the alloying elements, and identify a new important requirement to the design of radiation-tolerant alloys through modification of the composition.

Keywords:

Electron microscopy; Irradiated metals; Phase transformation; Segregation; Single-phase concentrated solid solution alloys.

1. Introduction

The development of fusion and Generation-IV fission reactors demands advanced structural materials that can retain their performance under harsh operating environments, such as high temperature and high irradiation dose [1,2]. With respect to these challenges, single-phase concentrated solid solution alloys (SP-CSAs), including high-entropy alloys (HEAs) [3-5], have attracted increasing interest due to their high strength and ductility, improved fracture toughness, retarded energy dissipation, and suppressed damage accumulation [6-9]. These promising mechanical and physical properties rely on the extreme compositional complexity of this novel class of alloys, in which multiple principal elements (often in an equiatomic ratio) are randomly mixed in a simple crystal lattice. However, little is understood yet about the stability of such as-synthesized, high-entropy configurations under extreme environments, which are crucial to the reliable and predictable performance of these alloys in potential nuclear energy applications. The mechanisms of defect dynamics, radiation-induced segregation (RIS), and phase transition in multi-component CSAs are also of scientific significance, wherein the majority of knowledge are hitherto limited to binary and very few ternary systems [10,11].

In particular, CrFeCoNi-based equiatomic alloys have been extensively investigated as one of the few HEAs that can solidify as single-phase solid solution with a face-centered cubic (FCC) structure [4,6,8,12]. While long-range chemical ordering was confirmed to be absent after homogenization [13-15], the stability of such alloys under prolonged anneals [16,17] and electron/ion irradiations [18,19] still needs to be determined. For instance, a coarse-grained CrFeCoNiMn alloy was reported to decompose into three distinct phases: a body-centered cubic (BCC) Cr-rich solid solution, a B2-type FeCo, and a L1₀-type NiMn, after annealing at 500 °C for 500 days, but remained stable after annealing at 900 °C for 500 days [17]. Similar decomposition occurred in a nanocrystalline (with grain sizes of ~50 nm) CrFeCoNiMn alloy produced by high-pressure torsion, but after annealing at 450 °C for 15 hours [16]. On the other hand, a nanocrystalline (with grain sizes of ~10 nm) CrFeCoNiCu alloy was reported to retain its primary phase, i.e., FCC solid solution, when irradiated by 2 MeV electrons at 25 °C and 500 °C

up to a damage level of 40 displacements per atom (dpa), although BCC solid solution, B2-type FeCo, and L1₀-type NiFe phases were formed earlier [18]. No phase change was noticed in a coarse-grained CrMnFeNi alloy irradiated by 5.8 MeV Ni⁺ ions at 400~700 °C up to 10 dpa, while solute segregation was observed at grain boundaries [19]. Grain boundaries not only serve as sinks for the annihilation of radiation-induced defects [20], but also short paths for the biased diffusion of alloying elements [19,21], thus, they may be either beneficial or detrimental to the stability of SP-CSAs. In this regard, here we focus on the intrinsic segregation of single-crystalline or coarse-grained, equiatomic CrFeCoNi, CrFeCoNiMn, and CrFeCoNiPd alloys under high-voltage electron irradiations in which point defects but not displacement cascades are generated. The enrichment and depletion of alloying elements at radiation-induced dislocation loops as well as the embryos of phase decomposition within irradiated matrix are quantified using a scanning/transmission electron microscope (STEM). The factors that govern the nature and mechanisms of RIS in SP-CSAs are discussed.

2. Experimental

The three alloys studied in this work were synthesized using high-purity (>99.9%) elemental metals by arc melting and drop casting into copper molds. Single-crystalline CrFeCoNi was then obtained by directional solidification in a floating zone furnace under an Ar gas atmosphere [22], while CrFeCoNiMn and CrFeCoNiPd with very coarse grains over 500 μm were obtained by homogenization at 1200 °C for 1 week [23]. Disks with a diameter of 3 mm were thinned to electron-transparency by twin-jet electropolishing using an electrolyte of 10% perchloric acid + 90% ethanol at a temperature of −30~−20 °C and a voltage of 14~16 V. Irradiations by 1250 kV electrons were carried out inside a JEOL JEM-1300NEF high-voltage electron microscope at a nominal temperature of 400 °C. The steady temperature increase due to electron irradiation was estimated to be within 30 °C (see Appendix A for details). A damage level of 1 dpa was obtained by approximately 30 minutes of irradiation with an electron dose rate of $\sim 5 \times 10^{18} \text{ e} \cdot \text{cm}^{-2} \cdot \text{s}^{-1}$. All irradiations were conducted in areas with a normal close to [001] zone axis (ZA). Post-mortem

characterization of dislocation loops was performed using a FEI Tecnai TF-30 TEM operating at 300 kV. The Burgers vector (**b**), habit plane, and nature of each loop was identified using the $\mathbf{g} \cdot \mathbf{b}$ invisibility criterion and the inside-outside contrast method under variant ($\mathbf{g}$, $3.1\mathbf{g}$) weak-beam dark-field (WBDF) conditions, as described in our previous work [24]. Compositional profiles at dislocation loops and in the irradiated matrix were measured by energy dispersive spectroscopy (EDS) attached to a FEI TITAN STEM operating at 200 kV.

3. Results and Discussions

3.1. Structure of dislocation loops

The structure of defects in CrFeCoNi as induced by 1250 kV electron irradiation at 400 °C and their growth behavior up to 1 dpa has been described previously [24]. As represented in Fig. 1(a), two distinct types of defects, i.e., elliptical Frank loops with $\mathbf{b} = \langle 111 \rangle / 3$ and rhombus perfect loops with $\mathbf{b} = \langle 110 \rangle / 2$, were identified under WBDF imaging conditions. All dislocation loops were of interstitial-type [24], with the (apparent) habit plane perpendicular to **b**. While edge-on view of Frank loop (Fig. 2(a)) shows the flat $\{111\}$ habit plane, perfect loop (Fig. 2(c)) might possess non-planar configuration composed of alternating $\{111\}$ planes, since the $\{110\}$ habit plane is not close-packed in FCC lattice. This can be implied by the formation of perfect loops, with similar crystallographic characters but of vacancy-type, in quenched Al-based alloys [25] via the dissociation and reorientation of Frank loops [26]. We also note that Fig. 2(a) and 2(c) (and all STEM images hereinafter) were recorded in annular dark-field (ADF) mode, in which the contrast is sensitive to atomic mass (*Z*) but is also contributed by the scattering of lattice defects.

Fig. 1(b) and 1(c) show the representative defect structure in CrFeCoNiMn and CrFeCoNiPd, respectively, which were irradiated at the same conditions as of CrFeCoNi (1250 kV electrons, 400 °C, 1 dpa). Still, all dislocation loops were of interstitial-type. Perfect loops were present at a lower fraction in these quinary alloys, possibly due to the reduction in stacking fault energy [27]. The number density of loops was much lower, although the loop sizes were larger, in

CrFeCoNiMn and CrFeCoNiPd as compared to CrFeCoNi. While no evidence has been found for the difference in the displacement threshold energy of these complex alloys, the lower density of loop nucleus can be attributed to the enhanced recombination of point defects associated with the oversized elements (Mn or Pd) [28]. A detailed quantitative analysis of loop growth behavior will be presented elsewhere, and the following section (3.2) will focus on the nature of RIS at loop habit planes. In addition, one may notice the more “noisy” background in Fig. 1(b) and 1(c), which will be related in later sections (3.3 and 3.4) to the early stage of phase decomposition in the electron-irradiated matrix of CrFeCoNiMn and CrFeCoNiPd, respectively.

3.2. RIS at dislocation loops

Fig. 2(b) and 2(d) show the compositional profiles across the habit plane of a Frank loop and a perfect loop (with major axis lengths of 70~100 nm) in CrFeCoNi, respectively. Both types of loops showed a depletion of Cr and Fe along with an enrichment of Co and Ni to a comparable level of 2~3 at. % relative to the composition of irradiated matrix, which was identical to that of un-irradiated matrix. Segregation was observed within a wider range across the perfect loop, probably due to its atomically wavy configuration. RIS at defect sinks (e.g., dislocation loops and grain boundaries) has been modeled based on the fact that the migration of interstitials and vacancies in alloys can be chemically inhomogeneous [11]. While direct assessment of atomic diffusion in CrFeCoNi-based alloys has not been reported, Fig. 2(b) and 2(d) accord with recent molecular dynamics simulations of $\text{Ni}_{0.5}\text{Fe}_{0.5}$ and $\text{Ni}_{0.8}\text{Cr}_{0.2}$ concentrated FCC alloys [29,30], which showed that the interstitial diffusion was predominantly contributed by Ni, thus leading to the enrichment of Ni at the interstitial-type Frank loops formed by the accumulation of point defects. RIS behavior of CrFeCoNi also agrees well with the interstitial-binding mechanism as in binary alloys [31], which is governed by the atomic size difference (Δa) between the alloying elements. Thereby, the larger Cr/Fe atoms were not favored, while the smaller Co/Ni atoms were favored at the interstitial-type loops. The relatively small Δa in CrFeCoNi (see Table 1 [32]) was also responsible for the weak RIS as observed.

We further demonstrate that RIS in CSAs can be more complicated and dependent on the species of alloying elements. Fig. 3(a) and 3(c) show edge-on view of a Frank loop (with major axis lengths of 120~150 nm) in CrFeCoNiMn and CrFeCoNiPd, respectively, and Fig. 3(b) and 3(d) show the compositional profiles across the habit planes. Intriguingly, while a depletion of Mn/Pd and an enrichment of Co was observed to a significant level of 5~7 at. % relative to the un-irradiated matrix, the depletion of Cr/Fe and the enrichment of Ni was much weaker in CrFeCoNiPd, and was even unresolvable (i.e., below error bars) in CrFeCoNiMn. Although the depletion of Mn/Pd at interstitial-type loops can still be rationalized by their large atomic sizes (see Table 1 [32]), the distinct enrichment of Co and Ni indicated that RIS was not solely governed by Δa . The enthalpy of mixing (ΔH_{mix}) between all relevant elements, as calculated in equiatomic binary alloys [23,32,33], are further listed in Table 1. We notice that Ni-Mn possess a very negative ΔH_{mix} corresponding to a strong tendency to coexist, while their large Δa conversely requires a segregation at dislocation loops. This competition might eventually neutralize the variation of Ni concentration. Along this line, the significant segregation between Co-Mn could be attributed to their large Δa overcoming a less negative ΔH_{mix} . For CrFeCoNiPd, the large Δa between Co/Ni and Pd coincides with the positive (or near-zero) ΔH_{mix} , which favors their segregation at dislocation loops. Even so, the weaker segregation between Ni-Pd than Co-Pd was contrary to the more positive ΔH_{mix} . The weak depletion of Cr was also not well reasoned in view of the very negative ΔH_{mix} between Cr-Pd. Overall, further experimental and theoretical efforts are required for the quantification of RIS behaviors in multi-component CSAs, which could not be simply assessed by the combinations of their binary/ternary subsystems.

3.3. RIS in irradiated matrix of CrFeCoNiMn

In the remainder of this paper, RIS in the electron-irradiated matrix of SP-CSAs provides a unique probe to the configurational energy landscape of these complex alloys, since the embryos of phase transition (if any) are more likely to survive in the absence of displacement cascades and away from external defect sinks. To start with, CrFeCoNi did not present any observable

phase change up to 1 dpa (see Appendix B for details). In contrast, the irradiated matrix of CrFeCoNiMn showed grainy contrast in the Z-sensitive ADF-STEM image (Fig. 4(a)), and the corresponding selected area diffraction pattern (SADP) showed weak but certainly visible $\{100\}$ and $\{110\}$ families of reflections (Fig. 4(b)) that are forbidden for a disordered FCC lattice, indicating the emergence of long-range chemical ordering as induced by electron irradiation. In comparison, the un-irradiated matrix, which was away from the illumination of high-voltage electrons but was also annealed along with the irradiated matrix (the difference in temperature due to electron irradiation was insignificant, see Appendix A), merely showed slight oxidation on the surface of the TEM foil (marked by arrows in Fig. 4(c), the lattice-like contrast came from Moiré interference between FCC matrix and the spinel-type oxides, see Fig. 4(d)).

To assess the chemical nature of ordering, we further quantified the degree of covariance (DOC) between each pair of elements (A-B) in CrFeCoNiMn, which is defined as:

$$DOC = r_{A-B} \frac{\sigma_A}{\mu_A} \frac{\sigma_B}{\mu_B}. \quad (1)$$

Practically, composition of a specific region (i.e., irradiated or un-irradiated matrix) was measured by EDS at multiple random locations. Hence, μ_A (μ_B) and σ_A (σ_B) are the mean value and standard deviation of the atomic concentration of element A (B), respectively, and r_{A-B} is the Pearson correlation coefficient between the two elements. As seen in Fig. 5(a) and 5(b), standard deviations of all elements were increased due to electron irradiation. However, only Cr-Fe and Ni-Mn show a dramatically augmented and positive DOC, indicating spatial separation between these two pairs of tightly coupled elements (Co was not actively involved in any coupling). The covariance of Ni-Mn can be attributed to their very negative ΔH_{mix} [23,32] (see Table 1), and accorded well with previous reports that CrFeCoNiMn was decomposed by annealing at intermediate temperatures, generating a $L1_0$ -type ordered NiMn phase [14,17]. In the meantime, the $\{100\}$ and $\{110\}$ extra spots in Fig. 4(b), with the intensity (I) showing $I_{\{100\}} > I_{\{110\}} > 0$, can only be explained by a mixture of $L1_0$ -type ordered domains with the three different orientations (see Fig. 4(e)), although it is still unclear why ordering along $[001]$ orientation, which was close

to the normal of TEM thin foil, was not favored. Other major types of ordered structures, such as $L1_2$, B2, and σ -phase, can be further excluded by examining their SADPs in [001] ZA (see Fig. 4(f-h)), as calculated based on kinematical approximation [34]. For instance, $L1_2$ phase yields $I_{\{100\}} \sim I_{\{110\}}$, B2 phase yields $I_{\{100\}} < I_{\{110\}}$, and each $L1_0$ domain only provides a part of extra spots. Overall, we conclude that high-voltage electron irradiation induced a $L1_0$ (NiMn)-type ordering decomposition in CrFeCoNiMn, which supports the conjecture that SP-CSA (i.e., the high-entropy configuration) may not always be the energetically stable state, especially at intermediate temperatures and under irradiations, and that ΔH_{mix} may play a greater role in governing the phase stability of multi-component alloys [23].

3.4. RIS in irradiated matrix of CrFeCoNiPd

The electron-irradiated matrix of CrFeCoNiPd also manifested intriguing decomposition behavior. Unlike the spatially dispersed ordering in CrFeCoNiMn, a self-organized, tweed-like microstructure with modulated contrast along [100] and [010] directions was noticed in ADF-STEM image (Fig. 6(a)), and streaks along the same directions were observed in all diffraction spots in [001] ZA (Fig. 6(b)). Moreover, transverse splits along $[\bar{1}01]$ direction were observed for the spots with larger $|\mathbf{g}|$ (i.e., the length of reciprocal vector) in [101] ZA, while those with smaller $|\mathbf{g}|$ still showed longitudinal streaks along [010] direction (Fig. 6(c)). These features indicate that the structural modulations, and consequently the streaks of all reciprocal sites, were along all six $\langle 001 \rangle$ directions in three-dimensional reciprocal space, as illustrated in Fig. 6(g). In comparison, the un-irradiated matrix did not present any directional variation of contrast (Fig. 6(d)), nor diffuse intensity in SADPs (Fig. 6(e) and 6(f)).

The tweed-like microstructure was further associated with a segregation between Co/Ni and Pd. As demonstrated in Fig. 7(a) and 7(b), the regions rich of Co/Ni and Pd correlated well with darker and brighter contrast in the Z-sensitive ADF-STEM image, respectively. Cr/Fe were not significantly modulated compared to the un-irradiated matrix. Assuming Vegard's law [35], the variation of lattice parameter due to the segregation between Co/Ni and Pd was no larger than $\pm$

0.3 %. Nonetheless, the $\langle 001 \rangle$ -oriented streaks in SADPs, which were up to $\pm 3\sim 5\%$ of $|\mathbf{g}_{200}|$, can be modeled by a quasi-periodic modulation, e.g., spinodal decomposition, to the atomic scattering factor. This is herein simplified as a one-dimensional sinusoidal wave, $A \cdot \sin(2\pi x/\lambda)$, with a wavelength $\lambda = 5$ nm and a relative amplitude $A = 0.2$, as indicated by Fig. 7(a) and 7(b), respectively. Diffraction profile along each $[001]$ direction can be thus calculated based on the following Fourier transform [36]:

$$I(g) = \left| \mathbf{F} \left\{ U_0\left(\frac{x}{a}\right) \cdot \left[1 + A \cdot \sin\left(\frac{2\pi x}{\lambda}\right) \right] \right\} \right|^2 = I_0(g) + A^2 \cdot \left[I\left(g - \frac{1}{\lambda}\right) + I\left(g + \frac{1}{\lambda}\right) \right]. \quad (2)$$

Here, $U_0(x/a)$ and $I_0(g)$ is the atomic potential and diffraction of FCC lattice without modulation. As shown in Fig. 7(c), the diffuse intensity on the shoulder of experimental $\{220\}$ peak was exposed by deconvolution as a pair of extra peaks centering at $\sim 0.2 \text{ nm}^{-1}$, according well with the calculated diffraction of spinodal decomposition.

Tweed-like microstructure and streaks in SADPs were recognized as the signature of shear-coupled, pre-martensitic transformation in various FCC- and BCC-based ordered alloys [37-39], however, all along $\langle 110 \rangle$ directions. For instance, $\langle 110 \rangle$ -oriented tweeds appeared in a $\text{Fe}_{0.506}\text{Pd}_{0.494}$ alloy in the initial state of ordering transformation from FCC to L1_0 structure [37]. By contrast, spinodal decomposition in cubic crystals with an elastic anisotropic ratio $A = 2C_{44}/(C_{11}-C_{12}) > 1$, such as Ni and Pd [40], was known to self-organize along the soft $\langle 001 \rangle$ directions [41]. Although spinodal decomposition was not reported in Co-Pd and Ni-Pd phase diagrams at 400 °C [42], multi-component CSAs might possess ΔH_{mix} values that are different from their binary subsystems. Moreover, X-ray diffuse scattering measurements indicated that equiatomic Ni-Pd solid solution, which was homogenized at 1100 °C for 1 week, still contained $\langle 001 \rangle$ -oriented segregating clusters with lengths of 2~5 unit cells [43], reflecting the role of a positive ΔH_{mix} [33]. These might serve as the nucleus for spinodal decomposition, which was further prompted by the point defect flows generated by electron irradiation [44], and finally evolved into the quasi-periodic microstructure seen in Fig. 6(a).

4. Discussions

4.1. Governing mechanisms of RIS and the effect of damage type

Our comprehensive S/TEM characterization of electron-irradiated CrFeCoNi, CrFeCoNiMn, and CrFeCoNiPd alloys provides unique understanding of the mechanisms of RIS both at the defect sinks and within the intrinsic matrix. While various criteria have been proposed for the stabilization of single-phase solid solution in HEAs based on Δa and ΔH_{mix} between the alloying elements [45,46], we have shown above that the nature of RIS can be rationalized by the same sets of parameters, at least on a qualitative level. First, Δa plays a dominant role in determining the enrichment vs. depletion of alloying elements at the dislocation loops associated with a local stress field, with the only exception of Ni in CrFeCoNiMn, when the thermodynamic binding between Ni-Mn is very strong (we note that the segregation between Co-Mn is still determined by their large Δa). Meanwhile, phase instability of the electron-irradiated matrix can be triggered by ΔH_{mix} of a specific element pair, even if single-phase solid solution is still favored by the overall mixing enthalpy $\Omega = \sum_{i \neq j} 4\Delta H_{\text{mix}}^{i-j} c_i c_j$, e.g., when $-12 \text{ kJ/mol} \leq \Omega \leq 3 \text{ kJ/mol}$, in the as-synthesized state [46]. For instance, the ordering decomposition in CrFeCoNiMn is driven by the very negative ΔH_{mix} between Ni-Mn, and the spinodal decomposition in CrFeCoNiPd is driven by the positive ΔH_{mix} between Co/Ni and Pd. By contrast, CrFeCoNi, with all element pairs satisfying $-7 \text{ kJ/mol} \leq \Delta H_{\text{mix}} \leq 0$, remains stable up to 1 dpa. Therefore, a new and stricter criterion may exist for the stabilization of SP-CSAs under irradiation environments.

It is also valuable to discuss the nature and mechanisms of RIS under the damage of different types of particles, e.g., electrons, protons, heavy ions, and neutrons. Grain boundaries of several austenitic stainless steels presented RIS with identical features, i.e., enrichment of Ni and depletion of Cr, and comparable magnitude under varied irradiation conditions [28,47-49]. However, there have not been sufficient experimental results on the RIS of HEAs, regardless of damage type. A recent study of $\text{Cr}_{18}\text{Mn}_{27}\text{Fe}_{27}\text{Ni}_{28}$, a non-equiatomic SP-CSA with a FCC structure [19], showed an enrichment of Ni by ~5 at. % along with a depletion of Mn by ~5 at. % and Cr/Fe by ~2 at. % at grain boundaries when irradiated by 5.8 MeV Ni^+ ions at 500 °C up to

10 dpa. These features can be well explained by the interstitial-binding mechanism, as governed by Δa (see Table 1), or the inverse Kirkendall effect [48], since grain boundary is also the sink of vacancy diffusion. However, it seems that RIS was not significantly influenced by the strong binding between Ni-Mn, and no phase change was noticed in the ion-irradiated matrix [19]. While RIS behaviors may depend on the species and concentrations of alloying elements, we propose that irradiations by heavy ions, which generate far-from-equilibrium states (i.e., displacement cascades) on a much larger spatial and temporal scale compared to electrons [50], may suppress the role of thermodynamic parameters, such as ΔH_{mix} . In consequence, the nature and magnitude of RIS may be primarily governed by the solute-coupled migration of point defects and clusters, which is further modulated by the concentrated alloying of SP-CSAs [51].

4.2. Resistance to RIS and the role of compositional complexity

We finally emphasize the role of compositional complexity in RIS-resistance, which is evaluated based on the relative magnitude of element enrichment and depletion at defect sinks (e.g., dislocation loops, grain boundaries, and free surfaces). Fig. 8(a) compares the electron-irradiated CrFeCoNi alloy in this study with common austenitic stainless steels [48,49,52-54] and several Ni-based dilute and concentrated binary alloys [55,56], which were irradiated under varied conditions and up to a similar damage level. The evolution of RIS as a function of temperature and damage level will be studied in future. Although the effectiveness of defect sinks may depend on their character (indeed, dislocation loops and grain boundaries showed comparable RIS behaviors [54]), CrFeCoNi unambiguously manifests an improved RIS-resistance, which can be attributed to the reduced mobility [30] and enhanced recombination [28] of point defects. This alloy also shows promising phase stability under irradiation, and our results of CrFeCoNiMn and CrFeCoNiPd (also see Fig. 8(b)) indicate that RIS-resistance may not always be monotonically improved by increasing the number of alloying elements. As a closing remark, radiation-induced structural modulation may impose an additional energy barrier to point defect migration, and further contribute to the radiation tolerance and physical (i.e.,

transport) properties of CSAs and HEAs [8,27]. The consequence of RIS to the comprehensive performance of these complex alloys should also be the focus of future studies.

5. Conclusions

In summary, mechanisms of RIS in CrFeCoNi, CrFeCoNiMn, and CrFeCoNiPd equiatomic alloys are experimentally revealed, to our knowledge, for the first time. Cr/Fe/Mn/Pd can deplete and Co/Ni can accumulate at radiation-induced dislocation loops, while the actively segregating elements are alloy-specific and primarily determined by the atomic size difference. While the electron-irradiated matrix of CrFeCoNi shows promising phase stability, CrFeCoNiMn and CrFeCoNiPd show $L1_0$ (NiMn)-type ordering decomposition and $\langle 001 \rangle$ -oriented spinodal decomposition between Co/Ni and Pd, respectively, as governed by the enthalpy of mixing. Nonetheless, a quantitative interpretation and prediction of RIS behaviors in multi-component CSAs based on the knowledge of their binary/ternary subsystems is still a great challenge. RIS-resistance of CSAs and HEAs is inherent to their compositional complexity, but also dependent on the species of alloying elements. Overall, our findings identify a new important requirement to the design of radiation-tolerant alloys through modification of the composition.

Appendix A. Steady temperature increase due to electron irradiation

The TEM thin foil under electron irradiation is approximated as shown in Fig. A. Electron beam with a radius R_e and an intensity J_e is uniformly irradiated onto and completely transmitted through the central area of the specimen with a uniform thickness. The thickness out of irradiated area gradually increases with the distance (r) to center (we note that the value of thickness is not needed in the following calculations). Heat flow is restricted in radial direction of the specimen with a thermal conductivity κ (i.e., assuming no heat dissipation into the vacuum), and the temperature (T) at outer radius (R_0) of specimen is the nominal temperature of irradiation experiments (T_0). The steady-state heat transfer equation in cylindrical coordinates is written as:

$$\kappa\left(\frac{d^2T}{dr^2} + \frac{1}{r} \frac{dT}{dr}\right) + J_H = 0, \text{ when } 0 \leq r \leq R_e; \quad (\text{A.1})$$

$$\kappa\left(\frac{d^2T}{dr^2} + \frac{1}{r} \frac{dT}{dr}\right) = 0, \text{ when } R_e \leq r \leq R_0. \quad (\text{A.2})$$

Here, J_H is the input power density determined as:

$$J_H = \frac{\rho Q J_e}{e}, \text{ where } \rho \text{ is the density of specimen, and } Q \text{ is the total stopping power for}$$

electrons. The solution of these equations is (see Fig. A):

$$T(r) = T_{\max} - \frac{J_H}{4\kappa} r^2, \text{ when } 0 \leq r \leq R_e; \quad (\text{A.3})$$

$$T(r) = T_0 - \frac{J_H}{2\kappa} R_e^2 \ln \frac{r}{R_0}, \text{ when } R_e \leq r \leq R_0. \quad (\text{A.4})$$

In the end, the maximum temperature increase is determined by:

$$T_{\max} - T_0 = \frac{\rho Q J_e R_e^2}{4\kappa e} \left(1 + 2 \ln \frac{R_0}{R_e}\right). \quad (\text{A.5})$$

For our experiments, $J_e = 5 \times 10^{18} \text{ e} \cdot \text{cm}^{-2} \cdot \text{s}^{-1}$, $R_e = 3 \text{ } \mu\text{m}$, and $R_0 = 1.5 \text{ mm}$. The density and stopping power of CrFeCoNi-based alloys are approximated as that of pure Ni, i.e., $\rho = 8.91 \text{ g} \cdot \text{cm}^{-3}$, and $Q = 1.37 \text{ MeV} \cdot \text{cm}^2 \cdot \text{g}^{-1}$ for 1250 kV electrons [57]. However, thermal conductivity of these CSAs was known to be significantly suppressed than that of pure Ni. For instance, $\kappa = (10.3 \sim 13.7) \text{ W} \cdot \text{m}^{-1} \cdot \text{K}^{-1}$ at 300 K [58]. These data yield a steady temperature increase of no larger than 30 K, which should not be significant since $T_0 = 673 \text{ K}$.

Appendix B. Electron-irradiated matrix of CrFeCoNi

Structural changes were not observed in the electron-irradiated matrix of CrFeCoNi (up to 1 dpa), as confirmed by the featureless ADF-STEM image (Fig. B(a)) and SADP (Fig. B(b)). The slight oxidation can be indexed as corundum-type oxides (such as Cr_2O_3). Nonetheless, the DOC was consistently negligible, even after irradiation, for all element pairs (Fig. B(c)). One should note that Fig. 5(b) and B(c) are plotted in the same scale.

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Figure 1

Fig. 1. Representative defect structure in (a) CrFeCoNi, (b) CrFeCoNiMn, and (c) CrFeCoNiPd as irradiated by 1250 kV electrons at 400 °C up to 1 dpa, all viewed in ($\mathbf{g}$, 3.1 $\mathbf{g}$) WDBF condition with $\mathbf{g} = (020)$ near $[001]$ ZA. The symbol of each dislocation loop denotes its Burgers vector.

Figure 2

Fig. 2. RIS at (a,b) Frank loop and (c,d) perfect loop in CrFeCoNi. (a,c) ADF-STEM edge-on views of the loops. (b,d) EDS line-scans across the habit planes, i.e., along arrows in (a,c). Error bar shows the standard deviation of composition at each measurement point.

Figure 3

Fig. 3. RIS at Frank loops in (a,b) CrFeCoNiMn and (c,d) CrFeCoNiPd. (a,c) ADF-STEM edge-on views of the loops. (b,d) EDS line-scans across the habit planes, i.e., along arrows in (a,c).

Figure 4

Fig. 4. Ordering in electron-irradiated matrix of CrFeCoNiMn. (a) ADF-STEM image and (b) corresponding SADP in $[001]_{ZA}$. Enlarged view of box highlights $\{100\}$ and $\{110\}$ families of extra spots. (c) ADF-STEM image and (d) SADP of un-irradiated matrix in $[001]_{ZA}$. Arrows in (c) and circles in (d) correspond to spinel-type surface oxides that are near-epitaxial to FCC matrix. (e) Simulated SADP yielded by a mixture of $L1_0$ -type ordered NiMn phase in all three orientations. (f-h) Simulated SADPs of other types of ordered (OD) phases with cubic/tetragonal structures: (f) $L1_2$ - Ni_3Mn ; (g) $B2$ -FeCo; (h) σ - $Cr_{1-x}Fe_{1+x}$. All SADPs are in $[001]_{ZA}$.

Figure 5

Fig. 5. Decomposition in electron-irradiated matrix of CrFeCoNiMn. (a) Correlation map of all element pairs in un-irradiated (open circles) and irradiated (solid circles) matrix as measured by EDS. (b) DOC of all element pairs. Concentrations of Ni-Mn (*) show a significantly augmented and positive covariance due to irradiation.

Figure 6

Fig. 6. Modulated structure in electron-irradiated matrix of CrFeCoNiPd. (a) ADF-STEM image and corresponding SADPs in (b) $[001]$ and (c) $[101]$ ZAs, respectively. Enlarged views of boxes highlight the streaks and splits of diffraction spots. (d) ADF-STEM image and (e,f) SADPs of featureless, un-irradiated matrix. (g) Schematic of $\langle 001 \rangle$ -oriented streaking in three-dimensional reciprocal space. Diffraction are calculated by intersecting reciprocal sites using Ewald sphere.

Figure 7

Fig. 7. Spinodal decomposition in electron-irradiated matrix of CrFeCoNiPd. (a) Enlarged ADF-STEM image shows no extra phase. (b) EDS measurements at alternating locations with bright and dark contrasts in (a). Shadow shows the compositional range of all elements in un-irradiated matrix. (c) Solid circles: intensity profile of {220} reflections along [100] direction (P-P) in Fig. 6(b). Dash line: intensity of central peak fitted by Lorentz distribution. Open circles highlight the diffuse intensity. Solid line: calculated diffraction profile (e.g., along Q-Q in Fig. 6(g)) of a one-dimensional sinusoidal wave with a wavelength (λ) = 5 nm.

Figure 8

Fig. 8. Magnitude of RIS, i.e., change of composition relative to that of un-irradiated matrix, at defect sinks. (a) Comparison between CrFeCoNi (in this study) and common austenitic stainless steels and Ni-based binary alloys as irradiated to similar damage levels and at temperatures around 400 °C. (b) Comparison between the three alloys in this study.

Fig. A. Schematic of a TEM thin foil (not plotted to scale) under electron irradiation and the calculation of steady temperature increase.

Fig. B. Electron-irradiated matrix of CrFeCoNi. (a) ADF-STEM image and (b) corresponding SADP in $[001]_{ZA}$. (c) DOC of all element pairs in the un-irradiated and irradiated matrix.

(010) ($\bar{1}10$)
L1₀ - NiMn