Characterization of Yttrium-Rich Precipitates in a Titanium Alloy Weld

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Abstract

The yttrium-rich (Y-rich) precipitates that form in the fusion zone (FZ) of a Ti–5Al–1Sn–1Zr–1V–0.8Mo (wt.%) alloy, or Ti-5111, gas-tungsten arc welds (GTAW) were characterized. The filler metal was modified by a small concentration of Y in order to refine the microstructure and thus improve the FZ ductility. A high number density of nanoscale Y-rich precipitates were characterized in the weld FZ by atom probe tomography (APT) and scanning transmission electron microscopy (STEM).

Keywords: Titanium; weld; yttrium; atom probe tomography (APT); high-angle annular dark field (HAADF)

1. Introduction

Titanium (Ti) alloys are technologically important for diverse applications in many industries, such as aerospace, biomedical, naval, and energy production [1,2]. One titanium alloy designed for structural marine applications is Ti-5Al-1Sn-1Zr-1V-0.8Mo (wt.%), which is referred to as Ti-5111 [3]. It has intermediate strength, excellent corrosion resistance, high toughness, excellent stress-corrosion cracking resistance, and room temperature creep resistance [3]. This alloy has a near- α microstructure that consists of colonies of hexagonal close-packed (h.c.p.) α -phase plates (or lamella) with small quantities of retained body-centered cubic (b.c.c.) β -phase grains between the plates [4,5]. The h.c.p. α -phase colonies have an orientation relationship (OR) such that their $\{0001\}$ basal planes are misoriented by 60° and share a common $\langle 11\bar{2}0 \rangle$ close-packed direction [5]. One limitation of this alloy is, however, that conventional welding processes may have a deleterious effect on the weld's ductility due to the embrittling effect of interstitial impurity elements, such as oxygen (O) [6,7], and the formation of coarse, columnar grains in the fusion zone (FZ) microstructure [8]. Oxygen atoms reside at the octahedral interstitial sites of the h.c.p. α -Ti lattice and act to strengthen the alloy thereby reducing its ductility and increasing its strength [6,7,9]. One approach to improve the weld ductility of alloys is microstructural refinement and sequestering of interstitial elements through compositional changes in the FZ by adding rare earth elements to the weld filler metal [10]. More specifically, Neuberger, et al.'s recent approach to improve the FZ ductility was to modify the weld filler metal by adding small concentrations of yttrium (Y) [11].

In earlier reported results, Neuberger, et al. [11] compared the mechanical properties and microstructure of Ti-5111 plates welded by filler metal matching the base metal (BM) composition, filler metal modified with 60 parts per million (ppm) Y, and filler metal modified

with 268 ppm Y when employing a gas-tungsten arc welding (GTAW) procedure. Their results indicated that the FZ of both yttrium-modified filler metal welds exhibited greater ductility (percent reduction in area) of 21.2 ± 1.0 % and 17.4 ± 6.4 %, when compared to the the FZ of the matching BM filler metal weld ductility of 14.8 ± 7.5 % and the BM ductility of 15.0 ± 3.3 % [11,12]. Additionally, Vickers microhardness measurements indicated that the FZ of both yttrium-modified filler metal welds exhibited a lower hardness when compared to the FZ of the matching BM filler metal weld [11,12]. They also measured an improved tearing modulus, T , meaning that the FZ of both yttrium-modified filler metal welds exhibited more stable crack growth once a crack was initiated. Furthermore, their scanning electron microscope (SEM) observations of the fractured tensile specimens indicated that both yttrium-modified filler metal FZ fracture surfaces were more characteristic of failure by microvoid coalescence and dimpled rupture, whereas the matching BM filler metal FZ fracture surface was more characteristic of cleavage failure [11,12]. Neuberger, et al. partially attributed this improved response to a smaller average grain diameter in the FZ of both yttrium-modified filler metal welds caused by the possible presence of Y-rich precipitates that inhibited columnar grain growth and promoted limited heterogeneous nucleation of the grains [11,12]. Their conventional transmission electron microscope (TEM) and selected area electron diffraction (SAED) pattern observations suggested the presence of small nanoscale precipitates in the FZ of the yttrium-modified filler metal welds that were not present in the FZ of the matching BM filler metal welds [11,12]. The crystal structure of the small precipitates could not, however, be definitively resolved, and their composition was not conclusively characterized. The authors suggested, however, that the precipitates were possibly face-centered cubic (f.c.c.) yttrium oxide (Y_2O_3) or trigonal yttrium oxysulfide (Y_2O_3S) based on the aforesaid observations and due to the strong affinity between Y

and O or S that is related to their electronic structure leading to large negative values of enthalpy of formation, ΔH_f , and even small concentrations can lead to the formation of oxides and sulfides [10,13,14].

This investigation characterizes the possible Y-rich precipitates that form in the FZ of the high yttrium-modified filler metal weld, which improve its ductility. We employ state-of-the-art atom probe tomography (APT) and scanning transmission electron microscopy (STEM) and report the first direct visualization of these precipitates and confirm that they are enriched in Y. The sub-nanometer spatial resolution and high elemental sensitivity of the APT technique [15] permits three-dimensional (3-D) visualization of nanoscale precipitates [16], while STEM permits analysis of a wider field-of-view (FOV) than APT via both high-angle annular dark-field (HAADF) imaging and x-ray energy dispersive spectroscopy (XEDS). We also discuss the local distribution of O and S in the weld FZ matrix phase and the Y-rich precipitates.

2. Experimental Procedures

2.1. Material

The nominal composition of the yttrium-modified filler metal containing 268 ppm Y and the base metal as measured by Timet Co. are given in Table 1. Details regarding the BM alloy plate fabrication and yttrium-modified filler metal fabrication are found in Refs. [11,12]. The BM had a nominal thickness of approximately 25.4 mm (1-inch). A summary of the GTAW procedure is presented here and additional details are also found in Refs. [11,12]. Welding was performed by Tricor Metals, Inc. The double-V butt weld joint was fabricated by GTAW inside a glove box using nominally pure (> 99.99 at.%) argon (Ar) shielding gas. A total of 12 weld

passes were performed on each side using a nominal arc voltage of ~15 volts (V), a nominal weld current of ~225 amps (A), and a travel speed of 3.4 mm s⁻¹ for each pass.

2.2. Atom Probe Tomography (APT)

Specimens with a needle-shaped geometry necessary for APT analysis were fabricated using a FEI¹ Nova 600 dual-beam scanning electron microscope/focused ion beam (SEM/FIB) instrument following standard lift-out and annular milling procedures [17,18]. The *in situ* site-specific specimen preparation technique was performed on metallographic mounts to take APT specimen blanks in the weld FZ. Details regarding fabrication of the mounts are presented in Refs. [11,12]. A platinum (Pt) protective layer was deposited over a region of interest (ROI) using established procedures. Annular milling was performed employing a 30 keV gallium ion (Ga⁺) beam and sequentially decreasing probe current following standard procedures after transfer of the ROI to silicon (Si) microtip posts with an Omniprobe Micromanipulator [19]. A low keV ion beam of 5 keV was allowed to raster over the specimen tip to remove material that had been damaged by the 30 keV Ga⁺ ion beam annular milling operation [20]. The final apex of the specimen tips had a radii of ~50 nm suitable for APT analysis.

A CAMECA Local-Electrode Atom Probe (LEAP[®]) 4000 instrument in the Si configuration was used to perform pulsed-voltage APT. Data acquisition was performed at a specimen tip base temperature of 70 K, a pulse frequency of 200 kHz, and a pulse-to-standing DC voltage ratio of 20% in order to promote field evaporation. The evaporation rate was maintained at a constant 0.5% or 0.005 ions per pulse. The background pressure was an ultra-

¹Certain commercial equipment, instruments, or materials are identified in this paper in order to specify the experimental procedure adequately. Such identification is not intended to imply recommendation or endorsement by the National Institute of Standards and Technology, nor is it intended to imply that the materials or equipment identified are necessarily the best available for the purpose.

high vacuum (UHV) of 1.1×10^{-8} Pa (8.1×10^{-11} Torr). Data reconstruction and analysis was performed using the CAMECA Integrated Visualization and Analysis Software (IVAS), version 3.6.6.

2.2. Scanning Electron Transmission Microscopy (STEM)

Specimens taken from the weld FZ were also prepared for analysis by STEM-HAADF imaging and XEDS elemental characterization using standard dual-beam SEM/FIB instrument lift-out techniques [21]. Analysis was performed using an FEI Titan 80-300 STEM operating at 300 kV and a probe current of approximately 0.1 nA. For XEDS analysis, the microscope was also equipped with an EDAX Sapphire r-TEM side-entry Si(Li) spectrometer with super ultra thin window, a nominal solid angle of collection of 0.1 steradians, an energy resolution of 134 eV as measured for the Mn-K $_{\alpha}$ x-ray peak, and an active detector area of 30 mm². The XEDS hyperspectral images were acquired using a higher probe current of 0.3 nA from a 300 nm $\times$ 250 nm area of the specimen that contained several precipitates. A 5 nm $\times$ 5 nm pixel size was used and the spectra were integrated for 1 s. Phase analysis was performed using the Sandia National Laboratory (SNL) Automated eXpert Spectral Image Analysis (AXSIA) multivariate statistical analysis software [22], and spectral analysis was performed using the National Institute of Standards and Technology (NIST) Desk Top Spectrum Analyzer (DTSA) II software [23].

3. Results and Discussion

3.1. Yttrium-rich (Y-rich) Precipitates

The APT reconstruction, Fig. 1(a), illustrates nanoscale spheroidal Y-rich particles (red isoconcentration surfaces) that are distributed in the weld FZ matrix phase (blue atoms) with a

high number density, N_v , of ca. 3.0×10^{24} particles m^{-3} , where the theoretical atomic density is ca. $42.5 \text{ atom nm}^{-3}$ for this Ti alloy, which is used to determine the volume. The FZ contains predominantly Ti atoms (blue), as discussed below. These particles have a mean spherical volume equivalent radius, $\langle r \rangle = 0.85 \pm 0.05 \text{ nm}$, where the $\pm 2\sigma$ error is given by standard error of the mean and the spheroid volumes are provided by interface analysis in the IVAS software. A normal probability plot, Fig. 1(b), demonstrates that these particles deviate from linearity that is expected of local statistical compositional fluctuations in a random solid-solution and thus these particles are stable Y-rich precipitates. Correlative STEM-HAADF imaging accompanied with XEDS elemental analysis was also performed in order to visualize the Y-rich precipitates in the weld FZ. The STEM-HAADF image in Fig. 2(a) illustrates nanoscale spheroidal areas of lighter phase contrast several of which are highlighted by black circles in a matrix of darker phase contrast that further demonstrates precipitates are distributed in the FZ microstructure. The observed contrast variation is indicative of differences in atomic masses, i.e. Z-contrast. A higher magnification view of an ROI (yellow square) encompassing a subset of the STEM-HAADF image in Fig. 2(a) also illustrates the nanoscale spheroidal precipitates, Figs. 2(b). An accompanying parallel STEM-XEDS data image illustrates that these are Y-rich precipitates (red) in the weld FZ (blue), Fig. 2(c). The accompanying XEDS spectra for the precipitates (red), Figs. 2(d) – (e), exhibits a Y- K_α peak at 14.931 keV and a Y- L_α peak at 1.922 keV, whereas the weld FZ (blue) does not exhibit a Y signal greater than the background noise. Thus, a second independent visualization technique, which is based on Z-contrast imaging, also illustrates that Y-rich precipitates exist in the weld FZ after the welding process.

Compositional analysis using proximity histogram (proxigram) [24,25] concentration profiles, Figs. 3(a) – (c), illustrate the distribution of Ti (blue circles), Al (teal inverted triangles),

Y (red diamonds), Sn (mustard triangles), Zr (green inverted triangles), V (gray circles), and Mo (purple squares) atoms in the FZ matrix phase and the precipitates. The O and S (light blue circles) concentration profile is also depicted in Fig. 2(b) and discussed below. The enhancement of Y in Fig. 2(b) permits discrimination of the precipitates at the right-hand side of the Ti matrix/Y-rich precipitate heterophase interfaces. Quantitative analysis of the precipitate and weld FZ Ti-matrix phase compositions are derived from the APT proxigram concentration profiles, Table 2. In this investigation, the plateau points within the matrix (far-field) yield the FZ Ti-matrix concentrations where the plateau points [26] are delineated by utilizing the Ti concentration profile as a fiducial marker. Only data points within the flat region of the profile, a minimum of 1.0 nm away from the heterophase interfaces and with $\pm 2\sigma < 0.2$ at.%, are included as plateau points. We consider here that the seven right-hand side points from the interfaces in Figs. 3(a) – (c) delineate the precipitate compositions. The partitioning ratio for an element i is defined as $\kappa_i^{ppt./mat.} = C_i^{ppt.} / C_i^{mat.,ff}$, where $C_i^{ppt.}$ is the precipitate composition and $C_i^{mat.,ff}$ is the far-field matrix concentration. The calculated partitioning ratios from the results in Table 2 are 0.98 for Ti, 1.04 for Al, 50.0 for Y, 1.0 for Zr, 0.9 for V, 0.8 for Mo, and 1.0 for Sn. The observed precipitates are strongly enriched in Y. The Y-rich precipitates are slightly depleted in V and Mo. Titanium exhibits a very small depletion while Al exhibits a very small enrichment in the Y-rich precipitates relative to the FZ α -Ti matrix. Yttrium exhibits limited solid-solubility in Ti, and its maximum solubility in h.c.p. α -Ti is significantly < 1 at.% at temperatures ≤ 870 °C [27]. Hence, it is possible that the Y-rich precipitates nucleate and grow by solid-state transformation during air-cooling of the weld FZ after completion of the welding process. The APT proxigram analysis of the precipitates illustrate that they are enriched in Y but also contain concentrations of Ti, Al, Zr, V, Mo, Sn, and O that are similar to that present in the weld FZ

matrix, Table 2. It is known, however, that precipitates with a radius of $< \sim 1$ nm may be influenced by elements from the matrix phase due to trajectory overlap and local magnification effects [28]. Hence, this limitation may prevent determination of the exact composition of the precipitates.

3.2. Oxygen and Sulfur

The nominal composition of O is 0.094 wt.% in the BM and 0.089 wt.% in the high-Y weld filler metal and S is present as a trace element and thus these elements are expected in the weld FZ. Wavelength dispersive spectroscopy (WDS) results indicated that both O and S are present in the weld FZ in Refs. [11,12]. In an APT mass spectrum, O, O₂, and S are, however, convoluted at a mass-to-charge state (m/n) ratio of 16 and also at a (m/n) ratio of 32 and thus the two elements are not readily distinguishable. Furthermore, the XEDS spectra could not delineate the presence of one element or the other due to convolution of the O-K _{α} peak at 0.523 keV with the Ti-L _{α} peak at 0.452 keV and the V-L _{α} peak at 0.510 keV, and the convolution of the S-K _{α} peak at 2.307 keV with the Mo-L _{α} peak at 2.293 keV. Hence, we assume that both elements may be present in the following discussion of the APT results.

The proximity histogram concentration profile in Fig. 1(b) illustrates that O and S are present in the weld FZ α -Ti matrix at a concentration of 0.3 ± 0.1 at.% and in the Y-rich precipitates at a concentration of 0.3 ± 0.03 at.%, Table 2. The calculated partitioning ratio is 1.0 indicating that O and S are equally present in the Y-rich precipitates and the weld FZ α -Ti matrix. The proxigram concentration profiles indicate, however, that local variation exists, particularly in the Y-rich precipitates and at the heterophase interfaces. A small O peak of 0.6 ± 0.2 at.% is located at a distance of 0.25 nm from the heterophase interfaces in the proxigram

concentration profiles. A second small peak of 0.4 ± 0.3 at.% is located at a distance of 0.45 nm from the heterophase interfaces. A depletion of 0.1 ± 0.05 at.% is located at a distance of -0.05 nm from the heterophase interfaces. Hence, in order to examine the distribution of O and S relative to Y in the FZ α -Ti matrix and Y-rich precipitates, we perform a concentration profile analysis of these elements averaged along the length of a 2 nm diameter cylinder with 1 nm bins at two different example locations in the reconstruction in Fig. 1(a). The concentration profiles illustrate visible enhancements of Y (red triangles) in each profile, Figs. 4(a) – (b), that correspond to Y-rich precipitates in Fig. 1(a). The O and S (light blue circles) profile illustrates that the local concentrations of these elements fluctuate in the FZ α -Ti matrix. Oxygen and S are also present in the Y-rich precipitates and at the FZ α -Ti matrix/Y-rich precipitate heterophase interfaces. The local O and S concentration at the interfaces is slightly greater than in the precipitates as demonstrated by the ~ 0.68 at.% and ~ 0.69 at.% peaks relative to the ~ 0.38 at.% concentration in the Y-rich precipitate in Fig. 4(a); and similarly, the ~ 0.94 at.% and ~ 0.90 at.% O and S peaks relative to the ~ 0.27 at.% concentration in the Y-rich precipitate in Fig. 4(b). The observed variability and fluctuations of O and S in the FZ α -Ti matrix are most likely due to the natural heterogeneity of the weld FZ microstructure [11,12] combined with non-equilibrium kinetics that occurs during welding and cooling. Differences in solidification rates and cooling rates during the welding process can lead to local heterogeneity in the microstructure and also varying time intervals for the effective diffusivity thereby leading to local variations and fluctuations in the O and S concentrations.

4. Conclusion

Atom probe tomography and STEM-HAADF imaging accompanied with XEDS elemental characterization were employed to characterize the Y-rich precipitates that improve the ductility of the weld FZ in a Ti-5111 alloy. The weld was fabricated by the GTAW procedure using filler metal modified with a small concentration of Y. This investigation resulted in the following findings:

- (1) A high number density, N_V , of ca. 3.4×10^{24} precipitates m^{-3} , of spheroidal Y-rich precipitates with a mean radius, $\langle r \rangle$, of 0.85 ± 0.05 nm were observed distributed in the FZ α -Ti matrix by APT. The calculated partitioning ratio of Y is 50.0 illustrating significant enhancement of Y in the precipitates.
- (2) Nanoscale spheroidal Y-rich precipitates were also observed distributed in the FZ α -Ti matrix by Z-contrast imaging accompanied with XEDS elemental analysis.
- (3) The O and S concentrations exhibit local fluctuations in the FZ α -Ti matrix and are also present in the Y-rich precipitates and at the α -Ti matrix/Y-rich precipitate heterophase interfaces.

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Table 1. Nominal compositions of the Ti-5111 base metal (BM) and yttrium-modified weld filler metal as reported in Ref. [11].

		Elements								
		Ti	Al	Y	Zr	V	Mo	Sn	O	C
High-Y Weld Filler Metal (FM)	(wt.%)	Balance	4.40	0.0268	1.00	1.00	0.75	1.00	0.089	-
	(at.%)	Balance	7.70	0.014	0.51	0.92	0.37	0.40	0.261	-
Base Metal (BM)	(wt.%)	Balance	4.92	-	1.05	1.00	0.80	1.00	0.094	0.009
	(at.%)	Balance	8.52	-	0.54	0.92	0.38	0.39	0.274	0.035

Table 2. Composition (at.%) of the nanoscale yttrium-rich (Y-rich) precipitates and the weld fusion zone (FZ) α -Ti matrix as measured by atom probe tomography (APT).

	Elements							
	Ti	Al	Y	Zr	V	Mo	Sn	O
Y-rich Precipitates' Composition	85.8 ± 1.0	8.8 ± 0.7	2.0 ± 0.3	0.5 ± 0.1	1.0 ± 0.2	0.4 ± 0.1	0.3 ± 0.1	0.3 ± 0.1
Weld FZ Ti- Matrix Composition	87.9 ± 0.2	8.5 ± 0.2	0.04 ± 0.01	0.5 ± 0.03	1.1 ± 0.1	0.5 ± 0.04	0.3 ± 0.03	0.3 ± 0.03
Concentrations are in at.%								
Concentrations do not total to 100 at.% due to rounding and the presence of Nb, C, and N trace and residual elements								

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Figure 1. Atom probe tomography (APT) reconstruction illustrating (a) the nanoscale spheroidal yttrium-rich (Y-rich) particles delineated by 0.25 at.% Y isoconcentration surfaces (red) in the weld fusion zone (FZ); and (b) the corresponding normal probability plot with a superimposed dashed line (blue) of a random binomial distribution. The reconstructed volume of $88 \text{ nm} \times 89 \text{ nm} \times 50 \text{ nm}$ in (a) contains approximately 7.3 millions ions. Only Y (red) and ca. 2.3% of the Ti (blue) atoms are shown for clarity in (a). The remaining elements are not shown for clarity.

Figure 2. Results of STEM analysis of the fusion zone (FZ) illustrating a STEM-HAADF image of the distribution of Y-rich precipitates in the FZ several of which are delineated by black circles, and a sub-region (yellow rectangle) analyzed by XEDS in (a). Depicted are the real-time HAADF output in (b) acquired simultaneously with the STEM-XEDS data in (c) that illustrates the spatial extent of the precipitate phase (red) and weld FZ matrix phase (blue) identified by multivariate statistical analysis. The accompanying XEDS spectra for the precipitates (red) and FZ matrix phase (blue) are shown in (d) and (e). For clarity, the spectral components are shown in two separate panels, one spanning between 0 keV and 10 keV and the other between 10 keV and 40 keV. The Cu peaks are due to the specimen holder.

Figure 3. The proximity histogram concentration profiles (at.%) derived from the reconstruction in Fig. 1(a) illustrating (a) Ti (blue circles) and Al (teal upside down triangles); (b) Y (red diamonds) and O and S (light blue circles); and (c) Sn (mustard triangles), Zr (green upside down triangles), Mo (purple squares), and V (gray circles) profiles.

Figure 4. One-dimensional Y (red triangles) and O and S (blue circles) concentration profiles (at.%) in (a) and (b) derived from two different 2-nm diameter analysis cylinders that illustrate Y enhancement (black arrows) corresponding to two different example Y-rich precipitates in the weld FZ from Fig. 1(a), and the associated local O and S distribution.