Formate Assisted Pyrolysis of Pine Sawdust for in-situ Oxygen Removal and Stabilization of Bio-oil

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Abstract

Pine sawdust was pretreated with several calcium compounds and then pyrolyzed in a fluidized bed pyrolysis reactor at 500 °C. The catalytic action of the calcium compounds varies depending on the anion. Analysis of pyrolysis gas, liquid and char yields and compositions demonstrates that calcium sulfate is inert during pyrolysis while calcium formate, carbonate, hydroxide and oxide show significant deoxygenation activity. Of the salts which showed deoxygenation activity, calcium formate had the highest relative yield. This effect is likely attributable to the activity of calcium formate as a hydrogen donor at the pyrolysis temperature.

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1. Introduction

Commercial production of renewable transportation fuels and chemicals from lignocellulosic biomass is hindered by both high capital and operating costs. The capital cost stems from small processing scales (relative to petrochemical) which are limited by the high biomass transportation costs. The operating costs reflect the natural resistance of woody biomass to decomposition, and the cost of removing oxygen while maintaining an economical product yield. Biomass pyrolysis has been identified as a process which can overcome the capital cost barrier, but the upgrading of the resulting bio-oil is still difficult and costly because the complex chemical and oxygenated nature of the oil requires a number of reactors, catalysts and significant amounts of hydrogen, while the product yield is relatively low (Hicks, 2011; Kakzeski *et al.*, 2010; Wildschut *et al.*, 2009). To date, the development of catalysts for post-treating bio-oil have been challenged by high coke/char yields and deactivation, due to the highly reactive nature of bio-oil (Mortensen *et al.*, 2011; Zacher *et al.*, 2014).

To reduce the burden of hydrotreating bio-oil from pyrolysis, methods such as catalytic pyrolysis have been demonstrated (Agblevor *et al.*, 2010; Mihalcik *et al.*, 2011). In catalytic pyrolysis, a zeolite catalyst is used during fast pyrolysis to promote cracking reactions that increase the C/O ratio and aromatics concentration (Carlson *et al.*, 2011). Oxygen is removed as CO₂ which reduces the carbon yield, yet does not require external hydrogen. While improvements in bio-oil quality have been reported, challenges such as process yields, catalyst regeneration and catalyst attrition remain. The composition of biomass limits mass yields because of the low H:C ratio of the starting material and the

tendency of carbohydrates to undergo dehydration and condensation (coke forming) reactions. The use of hydrogen as a carrier gas during catalytic pyrolysis (catalytic hydropyrolysis) has been shown to improve both the quality and yield of bio-oil by removing oxygen from the biomass as water, increasing the carbon yield in the liquid (Marker *et al.*, 2012; Meesuk *et al.*, 2011; Venkatakrishnan *et al.*, 2014).

As an alternative to zeolite-based catalytic pyrolysis, the effects of alkaline earth metal compounds on biomass pyrolysis have been explored by several groups. Wang, *et al.* mixed calcium hydroxide physically with pine at weight loadings up to 22% (Wang *et al.*, 2010). The authors found that the addition of the alkaline earth base slightly increased the overall yield while inhibiting the formation of acids, reducing the amount of sugars formed and increasing ketone and alcohol yields. Work by Lin, *et al.* mixing calcium oxide with loadings of 100-500% on pine also showed an increase in bio-oil yield accompanied by a decrease in oxygen content from 39 to 31 wt% at the highest loading (Lin *et al.*, 2010). Another recent study by Veses and coworkers demonstrated deoxygenation and decrease in acidity of bio-oil when calcium oxide and magnesium oxide were used as catalysts in an auger reactor (Veses *et al.*, 2014). Pyrolysis of magnesium oxide loaded cotton seed was studied by Pütün. The addition of oxide decreased the oxygen content by 50%, but unlike the calcium studies, bio-oil yield decreased with the addition of the alkaline earth metal (Pütün, 2010). The differing results between these studies illustrate the effect of reactor design and feedstock choice, as well as the pre-treatment process.

Recently, a simple and robust modification to the pyrolysis process was reported, which has the potential to reduce the complexity of upgrading the oil and increases process yields compared to catalytic fast pyrolysis. The process, called formate-assisted fast pyrolysis or FAsP, has been demonstrated on lignin (Mukkamala *et al.*, 2012). By pretreating the feedstock with calcium formate, a significantly deoxygenated bio-oil is produced in a single-step, atmospheric fast pyrolysis process.

In the current work, FAsP of pine (*pinus strobus*) sawdust was compared to conventional pyrolysis and several other calcium pretreatments. For all of the calcium pretreatments (with the exception of calcium sulfate), the oil quality was superior to conventional pine pyrolysis oil, having a significantly lower oxygen content, lower degree of polymerization and increased stability. Because the oil was less oxygenated, less hydrogen would be required for upgrading, thereby reducing the cost and complexity of downstream processing.

2. Materials and Methods

2.1 Feedstock Preparation

The calcium compounds were incorporated with the pine sawdust by forming a solution/suspension with the salt in deionized water, and then incorporating the dry sawdust. The mass loading of calcium was maintained constant for all experiments at 0.43 g calcium/g sawdust. This loading corresponds to the addition of 146 g calcium sulfate, 140 g calcium formate, 107 g calcium carbonate, 79 g calcium hydroxide and 60 g calcium oxide, respectively, each to 100 g pine sawdust. In all cases, the pretreated

pine was oven dried to 5-10% moisture and sieved to achieve particles smaller than 1.5 mm.

2.2 Pyrolysis

The pretreated sawdust was pyrolyzed with 40-60 mesh sand as heat transfer medium in a 3.5 cm x 30 cm entrained flow reactor described in detail elsewhere (DeSisto *et al.*, 2010). The reactor temperature was measured using two K-type thermocouples located on the vertical axis measured 3.0 and 9.5 in. from the top of the reactor. The pine/calcium formate mixture was metered through a screw feeder and pneumatically fed into the reactor, using a nitrogen flow rate of 6 L/min. The feed rate of the pretreated pine was approximately 1 g/min, and up to 1 kg of material could be processed in a run. The pyrolysis temperature was 500 °C. Immediately downstream of the reactor, char was separated using a hot gas filter (HGF) also maintained at 500 °C. The total vapor residence time in the fluidized bed reactor and the HGF was 12 sec, with about 90% of that time in the HGF. After the vapor passed through the hot gas filter the liquid was collected in a condenser operated at 6 °C, followed by an electrostatic precipitator (ESP) to collect aerosols. The gas exhaust from the ESP was periodically sampled and analyzed by GC. The exhaust gas flow rate was measured using a dry gas meter. Liquid yield was determined by weighing the condenser and electrostatic precipitator before and after pyrolysis. The char yield was determined by weighing the material collected in the reactor and the char filter, and then subtracting the mass of calcium compounds). The gas yield was measured using a dry gas meter. Each of the experiments was performed in duplicate, at minimum.

2.3 Characterization

2.3.1 Bio-Oil Characterization

The bio-oil analyses were conducted on oils collected from the electrostatic precipitator to ensure a water-free sample, as water can affect the results obtained from elemental analysis and size exclusion chromatography.

2.3.1.1 Elemental Analysis

Carbon, hydrogen and nitrogen analysis of the oil from the electrostatic precipitator was performed using a Thermo Scientific Flash 2000 elemental analyzer, and oxygen was calculated by subtracting the carbon, hydrogen and nitrogen from the total mass. This calculation has previously been compared to measured oxygen content using the same elemental analyzer and the difference method was found to be accurate for calculation of oxygen content for ash-free or low-ash samples.

2.3.1.2 Size Exclusion Chromatography

Size exclusion chromatography (SEC) was performed using an Shimadzu HPLC-GPC equipped with two columns measuring 1-1k Daltons and 1k-20k Daltons, respectively, with N,N-dimethylformamide (DMF) as the mobile phase. Due to the relatively low molecular weight of the oils produced with hot gas filtration, a large fraction of the sample elutes at the end of the calibration range with low resolution, making it difficult to quantitatively determine the molecular weight distribution and average molecular weight. Therefore, results from this method were used for comparative purposes only.

2.3.1.3 Quantitative Analysis by GC/MS

A Shimadzu Q2010 gas chromatograph-mass spectrometer (GC-MS) was used to characterize the composition of the oils. The samples were diluted with ethyl acetate solvent and prepared by adding butylated hydroxytoluene as a recovery standard and biphenyl as an internal standard. All of the samples were derivatized with N-Methyl-N-(trimethylsilyl) trifluoroacetamide (MSTFA) for one hour before analysis. Compounds reported were verified by both mass spectral fragmentation pattern and retention time matches to genuine standards.

2.3.2 Char Characterization

The solid product (containing char and inorganic compounds from the various calcium pretreatments) was analyzed by thermogravimetric analysis using a TA instruments Q500 TGA with a heating rate of 10 °C/min in a nitrogen environment.

2.3.3 Gas Characterization

The pyrolysis exhaust gas was measured using an SRI 8610C portable GC calibrated with a certified mixture of 1% methane, ethane, ethylene, acetylene, carbon monoxide and carbon dioxide in nitrogen.

3. Results and Discussion

3.1 Effect of Calcium Pretreatment on Pyrolysis Yields

The solid, liquid and gas yields, based on the starting pine sawdust mass, for each of the pretreated pine samples are shown in Table 1. The liquid yield represents the mass

collected in the condenser and electrostatic precipitator. The liquid was comprised of an organic fraction and aqueous fraction in the condenser, with only the organic fraction present in the ESP. The organic fraction was slightly denser and phase separated from the aqueous fraction.

A significant amount of gas was produced for all of the experiments, including from untreated pine sawdust. Previous work has shown that the presence of the hot gas filter results in more gas-forming reactions (Case *et al.*, 2014). The gas yield is lower for the calcium sulfate pretreated sawdust, than for the untreated pine which corresponds with the higher liquid yield observed for that pretreatment.

3.2 Effect of Calcium Pretreatment on Gas Composition

Calcium formate was used as a pretreatment compound because of its action as a hydrogen donor upon heating. When calcium formate is pyrolyzed at temperatures greater than about 450 °C, the formate salt decomposes to produce solid calcium carbonate and gaseous carbon monoxide and hydrogen.

If calcium formate simply decomposed without molecular interaction with pyrolysis intermediates, an overall gas yield of approximately 90 g/g pine would be expected, with about 52 g CO/g pine. However, the gas yield for calcium formate pretreated pine is only slightly higher than that of untreated pine, 59 vs. 57 g/g pine as shown in Figure 2. This comparison, as well as the increased organic yield observed with calcium formate pretreatment (Table 1), indicates that some fraction of both the hydrogen and carbon

being produced during calcium formate decomposition are being incorporated into the liquid pyrolysis product.

Calcium hydroxide and calcium oxide have a significantly lower gas yield when compared to untreated pine. Calcium hydroxide dehydrates to form calcium oxide, and with CO₂ present, the oxide likely sequesters some gaseous CO₂ in the solid product as carbonate. This hypothesis is supported by the specific decrease in CO₂ observed with these pretreatments. In contrast, the gas yield for the calcium carbonate pretreated pine is similar to that of untreated pine. This is not surprising considering the calcium exists as a carbonate both before and after the reaction, although its chemical nature during the reaction is not known since there is an observable effect on the pyrolysis oil composition.

3.3 Effect of Calcium Pretreatment on the Physical and Chemical Properties of Bio-oil

3.3.1 Elemental Analysis

The carbon, hydrogen and oxygen content, which are important for fuel quality, were determined for all of the organic liquids, and the results are presented in Table 2.

A significant decrease in O:C ratio results from pre-treatment with all of the calcium compounds except for calcium sulfate. The calcium sulfate increases the overall oxygen content and O:C ratio compared to untreated pine. For each of the other pretreatments, the oxygen content is decreased between 35-60%. For calcium formate pretreatment, no reduction in H:C ratio is observed, likely due to incorporation of formate-derived hydrogen, while pretreatment with carbonate, hydroxide and oxide cause a small

decrease. The carbon yield is increased for calcium formate pretreatment, compared to pyrolysis of untreated pine, indicating that carbon from the calcium formate may also be incorporated into the liquid product.

3.3.2 Chemical Composition from Quantitative GC/MS

The organic fractions of the oil products were analyzed by GC/MS. In each case, between 10-20% of the total oil was identified. This was limited because GC/MS is only able to detect compounds which have a minimum volatility, and preparing standards for each of the hundreds of detectable compounds is not practical or economically feasible since many are not available commercially. Trimethylsilyl (TMS) derivitization helps to improve the number of detectable compounds by increasing the volatility of hydroxylated compounds. Even so, high molecular weight compounds like polyaromatic hydrocarbons (PAH) and long-chain fatty acids are unaffected. Many low-molecular-weight acids and aldehydes are not quantifiable because of overlap with the solvent and MSTFA decomposition product peaks. Table 3 lists the most significant compounds identified by GC/MS. The percentage of the oil that can be quantified increases with calcium pretreatment, likely because more of the compounds are lower molecular weight phenolics. The exception to this is the untreated pine oil, which contains a large amount of levoglucosan, the cellulose anhydrosugar, which is quantifiable in GC/MS after derivitization.

Figure 3a presents the concentrations of major phenolic compounds identified by GC/MS. Major peaks include catechols, phenols and alkyl substituted catechols and

phenols. There is a shift from catechol-type compounds to phenol-type compounds when pyrolyzing calcium formate, carbonate, hydroxide or oxide pretreated pine. Additionally, these pretreatments also lead to increased alkylation of the phenolic compounds, increasing the relative concentrations of methyl-, C2- and C3- alkyl substituted phenols. The presence of alkylated phenols is consistent with the products of lignin FAsP where methoxy-phenols were observed to convert to alkylated phenols during oxygen removal (Mukkamala *et al.*, 2012). Additionally, cellulose has been shown to form phenolics under pyrolysis conditions (Byrne *et al.*, 1966), therefore some of the phenolics in the oil may originate from the carbohydrate fraction of the pine.

Five-membered rings such as furfural and 5-hydroxymethyl furfural (5-HMF) are common decomposition products of the hemicellulose fractions of biomass. When pretreatment with calcium formate, carbonate, hydroxide or oxide is applied, however, the furfural disappears and the concentration of substituted cyclopentenones significantly increases (Figure 3b). These results are consistent with the literature, which has shown that alkali compounds catalyze formation of substituted cyclopentenones (Di Blasi *et al.*, 2009). The source of these compounds has been hypothesized to be carbohydrates, however the same compounds were observed during FAsP of lignin, indicating that these compounds may be alkali catalyzed decomposition products of lignin monomers or linkages.

Another significant effect of calcium pretreatment is the decrease in anhydrosugars such as levoglucosan. This result is supported by literature, which has shown that alkali and

alkaline earth metals promote gas forming reactions over depolymerization and dehydration (Patwardhan *et al.*, 2010).

Another interesting result from calcium treatment is the presence of retene (1-methyl-7-isopropyl phenanthrene). Retene can be formed from dehydroabietic acid (one of the major resin acids found in pine). This transformation consists of decarboxylation, demethylation and dehydrogenation reactions and is not energetically favorable during conventional pyrolysis (Marchand-Geneste & Carpy, 2003). Almost complete conversion of dehydroabietic acid to retene is observed when calcium is added, however. This may be due to the decarboxylation potential of calcium. Decarboxylation has a high energy barrier, but if it can be catalyzed by calcium, the rest of the conversion to retene may occur. This reaction liberates 4 moles of H₂/mole dehydroabietic acid, potentially providing a native, in-situ hydrogen source.

3.3.3 Qualitative Stability Analysis by Size Exclusion Chromatography

One of the most significant characteristics of oils obtained from pine pretreated with calcium formate, carbonate, hydroxide or oxide is their stability compared to conventional pine bio-oil. Figure 4 presents SEC data for each of the oils before, during and after aging. The improved stability of these oils is likely attributed to the chemical changes in the oil, specifically reduced low oxygen content, which is typically directly correlated with stability. In addition to the increased stability, a shift in molecular weight distribution to the lower molecular weight region (relative to untreated pine pyrolysis oil) occurs with all of the calcium pretreatments except for calcium sulfate.

3.4 Potential Mechanisms for the Catalytic Activity of Calcium Pretreatment

During pyrolysis of mixtures of biomass/biomass constituents and alkali/alkaline earth metal salts many chemical and physical processes occur simultaneously. Depending on the salt used, different interactions will take place.

3.4.1 Transformations of Calcium Pretreatment Compounds During Pyrolysis

Calcium sulfate is very stable to extremely high temperatures, and does not appear to interact with the biomass at all. The increased mass yield and lower-quality oil produced from calcium sulfate pretreatment may have to do with the physical dilution of pine sawdust during pyrolysis, which may inhibit heat transfer and cracking reactions.

Although calcium carbonate is also quite stable to temperatures higher than those used for pyrolysis, this pretreatment has a significant effect on both the yield and quality of the oil. While the mechanism for this effect is not fully understood, similar results have been observed in the literature (Di Blasi *et al.*, 2009). Calcium hydroxide and calcium oxide both have the ability to sequester CO₂ from the gas phase, thus producing a more reducing environment. As in the case with calcium carbonate, however, the action of the cation is not yet fully understood. One potential effect is the in-situ neutralization of acidic compounds such as formic and acetic acid, which are known to cause instability in conventional pyrolysis oils (Diebold, 2000). Decarboxylation of organic acids is also possible, and evidence for this pathway is shown during the transformation of dehydroabietic acid to retene.

3.4.2 Incorporation of carbon and hydrogen from calcium formate

When calcium formate pretreated pine is pyrolyzed, the formate salt decomposes at approximately 450 °C to form carbonate, carbon monoxide and hydrogen (Mars *et al.*, 1963). It is possible that this decomposition causes the hydrogen (possibly radicals) to be generated within, or in the vicinity of, the solid particles. The hydrogen and carbon monoxide at this high temperature further reacts with the pyrolyzing biomass to remove oxygen, in-situ. The incorporation of hydrogen and carbon from the calcium formate with the biomass provides deoxygenation of the liquid product without a decrease in overall liquid yield or H:C ratio.

3.4.3 Effect of calcium pretreatment on carbohydrates

The lower liquid yields for pyrolysis of calcium pretreated pine relative to untreated pine correlate to decreased production of levoglucosan and other hemicelluloses derived anhydrosugars and furans. These carbohydrate pyrolysis intermediates responsible are a significant mass fraction of conventional pyrolysis oil, with levoglucosan making up about 60% of the total product obtained from pyrolysis of pure cellulose (Patwardhan *et al.*, 2010). Alkali and alkaline earth metals, however, have been found to promote pathways that favor cracking of cellulose to light oxygenates or formation of primary char (Kawamoto *et al.*, 2008; Kuzhiyil *et al.*, 2012). The elimination of anhydrosugars and furan compounds is not necessarily undesirable, however, as these compounds cause issues with downstream processing. They are highly oxygenated, include ring-bound oxygen and are very stable, making them poor

candidates for hydrodeoxygenation. During catalytic upgrading, the fate of most carbon and hydrogen bound in these compounds is as gas or coke (Kaldstrom *et al.*, 2011).

3.5 Implications for process economics

Pretreatment with inexpensive and recyclable compounds has the potential to transform present concepts of biomass conversion because it directly utilizes all biomass components (carbohydrates **and** lignin) for production of a stable, deoxygenated bio-oil with competitive yield in a single atmospheric fast pyrolysis step, which is compatible with the scale of biomass supply.

3.5.1 Effect of calcium pretreatment on capital cost for pyrolysis

This process generates oil with a similar yield and quality to that of catalytic fast pyrolysis, but has the potential to reduce the cost of pyrolysis because of the extremely low cost of calcium compounds. (Agblevor *et al.*, 2010; Carlson *et al.*, 2011; Mullen *et al.*, 2011). This simplifies the design of the pyrolysis reactor and reduces the capital cost.

3.5.2 Proposed process for calcium integration and recycle

Calcium sulfate and calcium oxide can be recycled after the char is burned off. Calcium carbonate can be formed by passing exhaust gas over the calcined oxide, and calcium hydroxide can be formed by slaking the calcined oxide. Calcium formate can be generated from the byproducts of pyrolysis, as outlined in Figure 5. Use of calcium oxide as the heat transfer medium makes recycle possible, since separation of solids is extremely difficult.

3.5.3 Effect of calcium pretreatment on downstream upgrading processes

Catalytic upgrading of pyrolysis oil is a necessary finishing step to produce a drop-in fuel. One obstacle to hydrodeoxygenation of bio-oil is its instability. Conventional bio-oil polymerizes over time and with increased temperature. Hydrotreating is generally performed at temperatures between 150 and 300 °C, at which bio-oil rapidly polymerizes. This leads to considerable char production and mass loss during upgrading. Oil produced by pyrolysis of calcium pretreated pine overcomes this issue by eliminating compounds that cause polymerization as well as compounds which do not contribute to the liquid product of upgrading. Hydrodeoxygenation of major compounds identified in the calcium pretreated pine oils has been proven in several studies (Wan *et al.*, 2012; Zhao *et al.*, 2011; Zhao *et al.*, 2010).

3.5.3 Comparison of calcium pretreatment processes

The choice of calcium compound for pyrolysis pre-treatment in a commercial-scale operation would be guided by economics. More analysis of the capital investment required for regeneration of calcium formate is necessary. The end-use application of the pyrolysis oil is also an important factor in determining the type of upgrading required and the capital and operating costs associated with that stage.

Conclusions

Pretreatment of pine with various calcium compounds has a significant effect on the physical and chemical properties of pyrolysis oil, including dramatically lowering the oxygen content of the oil and increasing its stability. This improvement in oil quality is

accomplished without external hydrogen or expensive catalysts in a single-step reactor, making it a simple, inexpensive and robust process. Additionally, the upgrading process burden is significantly reduced, lowering the cost required for fuel finishing. Among the calcium pretreatments employed, calcium oxide showed the highest percent deoxygenation in the liquid phase, while calcium formate showed significant deoxygenation without sacrificing bio-oil yield.

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Figure Captions

Figure 1. Thermogravimetric analysis of the solid product was used to calculate the amount of CO₂ released during decomposition of calcium carbonate (600-700 °C). This information, together with the known weight of calcium allows for determination of the ratio of oxide:carbonate in the solid product. As expected for calcium formate and calcium carbonate pretreatments, all of the calcium in the char is present as the carbonate. About 70% of the calcium hydroxide and 65% of the calcium oxide are converted to calcium carbonate by sequestration of CO₂.

Figure 2. Yields of non-condensable gas products from pyrolysis of pine sawdust and pretreated pine sawdust.

Figure 3. (a) Major phenolic products in the oils consist of catechols and phenols. Calcium pretreatment causes an increase in phenol-type compounds and a decrease in catechol-type compounds. (b) Five-membered rings present in the oils include furfural and substituted cyclopentenones. The degree of alkyl substitution increases when calcium pretreatment with formate, carbonate, hydroxide or oxide is employed.

Figures 4. Results of SEC analysis of the various calcium pretreated oils at different stages of aging.

Figure 5. Conceptual flow diagram for production of calcium formate from pyrolysis residue. Char from pyrolysis of calcium formate pretreated biomass can be gasified to produce carbon monoxide, which is then contacted with calcium hydroxide. Calcium hydroxide is regenerated by slaking calcium oxide, which is the resulting product of high temperature oxidation of calcium carbonate.

Table 1. Mass balances based on grams of reactant/product per 100 gram of pine fed

	Pine	CaSO ₄ Treated Pine	Ca(COOH) ₂ Treated Pine	CaCO ₃ Treated Pine	Ca(OH) ₂ Treated Pine	CaO Treated Pine
Water	7	15	12	10	18	17
Organic product	21	29	23	12	14	12
Char product*	12	11	36	17	21	13
Gas product	58	48	61	51	33	24
CaSO ₄ in solid product**	0	146	0	0	0	0
CaCO ₃ in solid product**	0	0	107	107	74	70
CaO in solid product**	0	0	0	0	18	21
Sum [†]	98	249	239	197	178	157
Mass Balance Closure	98%	101%	99%	95%	99%	98%

* On a calcium-free basis

** Refer to Figure 1 for more information about calcium compounds remaining in char

† For the pretreated pine cases, the sum is greater than 100 because it is calculated on a pine basis but includes the mass of the pretreatment compound.

Table 2. Properties of liquid products with and without pretreatment

	Pine Feed	Pine Oil	CaSO ₄ Treated Pine Oil	Ca(COOH) ₂ Treated Pine Oil	CaCO ₃ Treated Pine Oil	Ca(OH) ₂ Treated Pine Oil	CaO Treated Pine Oil
% Carbon (dry basis)	45.1	67.8	65.7	76.6	78.7	81.6	82.9
Carbon Yield	-	32	42	39	21	25	22
% Hydrogen (dry basis)	6.80	6.50	6.33	7.30	6.99	7.26	7.16
% Oxygen (by difference)	48.1	25.7	27.9	16.3	14.3	11.1	9.94
O:C (oil)	0.80	0.28	0.32	0.16	0.14	0.10	0.09
H:C (oil)	1.80	1.15	1.16	1.15	1.07	1.07	1.03

Table 3. Most abundant compounds quantified by GC-MS

Retention Time	Compound Identification	Concentration (µg/g)					
		Pine	Ca(SO ₄)	Ca(COOH) ₂	CaCO ₃	Ca(OH) ₂	CaO
6.9	Cyclopentenone	-	-	5,268	9,766	8,562	4,191
7.4	Furfural	2,207	4,816	-	-	-	-
10.4	2-methyl-2-cyclopenten-1-one	1,476	1,193	6,492	8,356	11,627	12,951
13.5	3-methyl-2-cyclopenten-1-one	2,790	2,804	6,143	10,326	11,207	11,659
15.3	Ethylene glycol	4,943	4,618	3,391	1,018	1,091	963
18.1	2,3-Dimethyl-2-cyclopenten-1-one	-	-	4,280	4,511	6,653	10,934
19.2	Phenol	6,105	6,798	8,668	16,920	21,126	32,610
19.9	Acetophenone	161		200	136	820	1,485
24.4	o-cresol	2,797	2,801	6,160	9,065	10,471	16,291
25.2	m-cresol	7,610	7,886	7,618	14,961	15,996	23,656
25.9	p-cresol	3,114	2,864	5,961	9,387	10,426	16,487
27.5	Napthalene	-	-	894	994	1,748	3,143
30.1	2,5-dimethylphenol	493	378	1,932	3,150	3,371	5,301
31.0	2,4-dimethylphenol	2,414	1,711	5,840	10,239	10,773	14,867
31.6	2,6-xlenol	-	-	1,674	1,027	1,408	1,709
32.0	4-ethylphenol	2,359	1,481	3,564	7,601	8,658	11,705
33.5	3,4-dimethylphenol	-	-	1,197	2,555	2,092	4,557
36.7	Hydroxyacetophenone	740	317	946	1,596	1,823	3,626
37.4	Catechol	38,441	33,371	17,306	9,323	7,789	1,888
37.7	2,3,5 trimethylphenol	-	-	3,170	3,455	3,165	4,748
42.3	4-methylcatechol	23,383	23,023	14,920	9,248	7,723	1,485
42.9	3-methylcatechol	7,181	6,913	7,899	7,001	6,490	870
47.5	4-ethylcatechol	23,998	19,623	14,623	5,391	5,389	1,453
52.4	1-hydroxynapthalene	912	457	223	2,805	3,355	6,437
53.4	Benzoic Acid	3,242	2,266	3,042	1,024	775	-
53.9	1,2,3-trihydroxybenzene	597	274	263	229	-	-
54.1	2-hydroxynapthalene	891	419	1,952	4,372	5,443	9,740
58.6	1,2,4 trihydroxybenzene	946	673	427	471	-	-
66.6	Levogluconan	33,535	7,159	5,092	1,160	496	408
77.3	Retene	-	2,595	4,354	10,777	12,623	24,271
79.2	Dehydroabietic acid	6,489	1,215	1,024	-	-	-
79.8	Dihydroxycoumarin	-	-	2,712	7,473	13,599	15,774
	Percent of Oil Identified	0.18	0.14	0.14	0.17	0.18	0.23

Figure 1.

Figure 2.

Figure 3.

Figure 4

Figure 5.