Synthesis of High Capacity Cathodes for Lithium-Ion Batteries by Morphology-Tailored Hydroxide Co-precipitation

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Abstract

Nickel manganese hydroxide co-precipitation inside a continuous stirred tank reactor was studied with sodium hydroxide and ammonium hydroxide as the precipitation agents. The ammonium hydroxide concentration had an effect on the primary and secondary particle evolution. The two-step precipitation mechanism proposed earlier was experimentally confirmed. In cell tests, Li- and Mn-rich composite cathode materials based on the hydroxide precursors demonstrated good electrochemical performance in terms of cycle life over a wide range of lithium content.

Keywords: Lithium batteries, Hydroxide Co-precipitation, Ammonia, Cathode, Continuously stirred tank reactor CSTR.

Introduction

As one of the most promising cathode materials with high energy density, Li- and Mn-rich composites have been investigated for over 10 years.^[1, 2] However, this material suffers from the drawback that a tradeoff is needed between rate performance and volumetric energy density.

The routine procedure for the synthesis of the composite cathode material involves two steps^[3–12]: precursors are synthesized through co-precipitation reactions, then the precursors are lithiated through high-temperature solid state reactions. Previous studies suggested that the properties of the Li- and Mn-rich cathode materials are greatly affected by the precursor, specifically, the composition,^[2, 6, 13–16] particle morphology,^[10, 17, 18] and size distributions.^[19] Tailoring the precursor morphology is one effective way to tune the material to be a high power or high energy cathode.

Carbonate and hydroxide co-precipitations are the most popular methods to prepare the cathode precursors. Carbonate co-precipitations have the merits of facile morphology control and environmental friendliness.^[10] However, before the steady state of the continuous reaction is reached, the particle usually becomes so large that the synthesized cathode cannot deliver decent rate capacity.^[20] What is more, void layers between the adjacent rings in the onion-like particle morphology render the cathode materials too fragile to achieve high electrode density.

Hydroxide co-precipitation does not have the limitations mentioned above; however, it is much more complex than the carbonate process, especially when a high manganese content composition is involved, for the following reasons. First, hydroxide precipitation can result in different structures. For example, both $\text{Ni}(\text{OH})_2$ and $\text{Co}(\text{OH})_2$

can be α phase, β phase, or β_{bc} phase, which highly depends on the synthesis conditions.^[21–24] The most reliable phase for the synthesis of Li- and Mn-rich cathode materials is β phase because its structure is impurity and defect free. Second, Mn_3O_4 always coexists with manganese hydroxide during the various stages of cathode synthesis (e.g., co-precipitation, precursor washing, lithiation). This is because in $Mn(OH)_2$, Mn^{2+} can easily oxidize to Mn^{3+} and then becomes segregated in the form of mixed hydroxides.^[10, 25] Third, hydroxide primary particles tend to adopt lamellar or needle-like morphology, which poses a challenge in preparing densely packed secondary particles.^[26–28]

In this research, we studied the co-precipitation reaction with sodium and ammonium hydroxide for the formation of Li- and Mn-rich cathode materials, in particular, the effect of ammonia concentration on the growth of the primary and secondary particles. Although ammonia is widely used in precipitation reactions to (1) maintain a relatively stable PH, (2) achieve homogeneous distribution for different metal ions by chelating effect,^[10,27,29–31] our study is the first systematic investigation to highlight its function as precursor morphology tailor by tuning (1) primary particle morphology (2) the packing behavior of the primary particles to form loosely or densely packed secondary particle. Coin cell tests of cathodes fabricated by the hydroxide co-precipitation demonstrated reasonable electrochemical performance.

Experiments

Nickel sulfate hexahydrate ($NiSO_4 \cdot 6H_2O$), manganese sulfate monohydrate ($MnSO_4 \cdot H_2O$), sodium hydroxide ($NaOH$), and ammonium hydroxide ($NH_3 \cdot H_2O$) were used as the starting materials to synthesize $Ni_{0.25}Mn_{0.75}(OH)_2$ precursor in a continuously

stirred tank reactor (CSTR). The feed rate of the transition metal solution was fixed at 16ml/min, while the pumping rate of the base solution (mixture of NaOH and $\text{NH}_3 \cdot \text{H}_2\text{O}$) was controlled by a pH controller. The precipitation reaction was conducted at a constant temperature (60°C) and a fixed stirring speed (1000 rpm). An N_2 cover gas was introduced into the CSTR to prevent Mn^{2+} oxidation. The precursor materials were collected for two hours after 8 hours precipitation reaction. Longer reaction time may lead to better particle morphology and tap density, but determining the optimized reaction conditions is beyond the scope of this study.

The collected samples were washed with de-ionized water several times to remove residual sodium and sulfur species, then filtered and dried inside a vacuum oven set at 100°C for 24 hours. Finally, Li- and Mn-rich cathode materials, $\text{Li}_x\text{Ni}_{0.25}\text{Mn}_{0.75}\text{O}_{2.5+\delta}$ ($1.54 \leq x \leq 1.71$), were prepared through a solid state reaction between appropriate amounts of $\text{Ni}_{0.25}\text{Mn}_{0.75}(\text{OH})_2$ and Li_2CO_3 at 900°C for 14 hours.

The morphology and particle size distribution of the precursor and cathode materials were characterized with a cold field emission scanning electron microscope (SEM, Hitachi S-4700-II) and particle size analyzer (Cilas1090), respectively. Tap density of the precursor was measured with Autotap from Quantachrome. The crystal structures of the precursor and cathode materials were determined by powder X-ray diffraction (XRD) with a D5000 Siemens X-ray diffractometer, using a $\text{Cu-K}\alpha$ radiation source ($\lambda = 1.5406 \text{ \AA}$). The samples were scanned from $2\theta = 5^\circ$ to 80° at a rate of $0.1^\circ/20 \text{ s}$. The chemical compositions were determined with inductively coupled plasma-mass spectroscopy (ICP-MS, Agilent Technologies 7700 series).

Electrochemical characterizations were conducted in CR2032 coin-type cells. Cathodes were composed of synthesized Li- and Mn- rich cathode materials (80 wt%), acetylene black (10 wt%), and polyvinylidene difluoride binder (10 wt%). A slurry of this mixture was coated onto an aluminum foil and dried at 85 °C. The lithium cells were assembled inside a helium-filled glove box with lithium metal as the counter anode, Celgard 2325 membrane as the separator, and 1.2M LiPF₆ dissolved in ethylene carbonate and ethyl methyl carbonate (3:7 volume ratio) as the electrolyte. The cells were tested with a 2.0-4.6 V voltage window and a C/3 discharge current. (In our calculations, the 1 C rate is assumed to be equal to 200 mA/g.)

Results and discussion

Table 1 lists the experimental parameters used to synthesize Ni_{0.25}Mn_{0.75} (OH)₂ precursors. The only variation was the base solution composition. To explore the ammonia effect on the precipitation process, the molar ratio between sodium hydroxide and ammonium hydroxide (M_S/M_A) was gradually increased from 2:3 (experiment #1) to 4:1 (experiment #6). The tap densities of the dried precursors were also measured and are listed in Table 1. Most of the precursors have relatively low tap density (<0.84 g/cm³), except for that from experiment #2 (1.5 g/cm³).

The tap density of the powder material is a reflection of the secondary particle size distribution and the primary particle packing within secondary particles. We found that ammonia concentration has a direct impact on both of the secondary particle growth rate and the primary particle packing. Evolutions of D50 particle size for four M_S/M_A ratios are compared in Figure 1. Neither the low M_S/M_A ratio (2:3, red line in Figure 1) nor the high M_S/M_A ratio (4:1, black line in Figure 1) benefits the secondary particle

growth. After 10 hrs reaction, the D50 values were still under 10 μm for these two ratios. At $M_S/M_A=3:2$ (olive line in Figure 1), D50 values increased with reaction time and stabilized between 10 and 11 μm after 5 hr. Decrease of M_S/M_A to 1:1 significantly boosted the initial growth rate (blue line in Figure 1): D50 quickly reached 23 μm from the initial 8 μm in the first 4 hr, with an average growth rate of 4.28 $\mu\text{m/hr}$, after which, D50 rapidly shrunk to 9 μm and became stabilized at this size. One hypothesis is that when the agglomerates approach a critical size, the shear stress exerted on the agglomerates by the hydrodynamic motion becomes larger than the cohesive force among primary particles, and then the agglomerates break down to smaller fragments, resulting in smaller D50. Different stirring rates and agglomerate population densities within the reactor could affect the agglomeration growth rate significantly, which is beyond the purpose of this study and will be discussed in separate papers.

The above hypothesis is supported by Figure 2, which shows the particle size distributions of hydroxide precursors collected for six M_S/M_A ratios. Most of the histogram curves have maxima at 0.3 μm , 2 μm , and 10 μm , which correspond to -crystal nuclei, agglomerate fragments, and agglomerates, respectively. The peak intensity at 10 μm is much higher than those at 0.3 μm and 2 μm (see inset to Figure 2), indicating the precipitate is mainly in the form of agglomerates. The relatively sharp peaks at 10 μm also show that the agglomerates are narrowly distributed. A process involving two levels of particle agglomeration (1–2 μm and 10 μm) was proposed in our previous report.^[32] We concluded that even though the growth rates varied for experiments with different M_S/M_A ratios, the particle growth follows the same two-level agglomeration mechanism.

The effect of M_S/M_A ratio on the agglomerate morphology is shown by the SEM images in Figure 3. Both low (2:3) and high (4:1) M_S/M_A ratios led to loosely packed secondary particles with irregular morphology (Figures 3a and 3f, respectively). For M_S/M_A of 1:1, the agglomerates are spherical with a very narrow particle size distribution (Figure 3b), which can be attributed to the higher tap density of the precursor (see Table 1).

The various agglomerate morphologies are a result of the diverse packing behaviors of the primary particles synthesized with different M_S/M_A ratios. The SEM images in Figure 4 show the effect of ammonia content on the primary particle morphology. In general, all of the precursors are lamellar with a lateral dimension around 500 nm. When the ammonia concentration is low (Figures 4a and 4b), the primary particles are multi-layered plates with rough edges. With increase of M_S/M_A ratio from 2:3 to 1:1, the thickness of the nanoplates increased from ~50 nm to >100 nm, which increased the mass of the agglomerates, and thereby enhanced the chance of effective - collisions of agglomerates with the other agglomerates and reactor wall/agitator that can cause the agglomerate shape to be spherical. Further increase in M_S/M_A ratio up to 5:2 led to single-layer plates with smooth basal surfaces (Figures 4c to 4e). Their irregular edges are the result of particle disruption created by strong fluid shear forces in the CSTR. At the M_S/M_A ratio of 4, the primary particles became regular hexagonal plates (Figure 4f), which may relate to the anisotropic growth of the six-fold symmetric crystallites.

Two reaction paths were earlier proposed for the metal hydroxide precipitation in the presence of ammonia. One group of researchers stated that the metal ions in the solution first coordinate with ammonia to form a complex, and then slowly release into

the solution, where they react with hydroxyl group to form hydroxide precipitates.^[29, 33]

The step-wise reactions can be expressed as:

where T.M. is the abbreviation of transition metal (Ni, Mn in our case). Other researchers proposed that the hydroxide precipitation involves a dissolution-recrystallization process.^[34]

The precipitate is thus a result of dynamic equilibrium between the solid metal hydroxide and aqueous metal ammonia complex.

In order to verify these proposed growth mechanisms, we prepared base solutions with M_S/M_A ratio = 2:3, 1:1, and 4:1 (same as that in experiment #1, #2, and #6, respectively). We separately added 1 g of the dried precursor collected from experiments #1, #2, and #6 to the corresponding base solution and kept the solutions at 60 °C for over two hours under magnetic stirring. Subsequently, the three precursor-basic solution mixtures were vacuum filtrated, and the filtrated supernatants were collected and labeled as (1), (2), and (3) respectively. At the same time, $NiSO_4$ solution (green) and $[Ni(NH_3)_n]^{2+}$ solution (blue) were prepared as the color identities of Ni^{2+} and $[Ni(NH_3)_n]^{2+}$ (Figure 5). After 2 hours of aging, the color did not change for the three solutions, which indicates no obvious nickel dissolution in either the Ni^{2+} or $[Ni(NH_3)_n]^{2+}$ forms. In other words, the hydroxide precursor is more stable than the ammonia complex under the precursor synthesis conditions. Reactions (1) and (2) are thus believed to be the main reaction path for the co-precipitation.

The crystal structure of the $\text{Ni}_{0.25}\text{Mn}_{0.75}(\text{OH})_2$ precursors for the six base solutions was verified with powder XRD. As shown in Figure 6a, there are no obvious differences in the XRD patterns among the batches of precursors. The main structure of the precursors can be indexed based on the $P\bar{3}m$ space group. The minor peaks highlighted with arrows in Figure 6 correspond to a Mn_3O_4 phase (space group $I4_1/amd$), which is the result of Mn^{2+} oxidation. Select area electron diffraction confirmed the precursor was $\text{TM}(\text{OH})_2$ rather than TMOOH , which was discussed in detail in our previous study^[32]. The composite structure of the precursors indicates that even though N_2 cover gas was applied during the synthesis process, a certain amount of Mn^{2+} oxidized to Mn^{3+} during synthesis, washing, or drying. The dominant peak located at $2\theta = 19^\circ$ has a much higher intensity than the other peaks due to the anisotropic growth of the primary particles. The broad peaks between 35° and 40° , according to previous reports, relate to stacking faults along the c -axis for the metal hydroxide, which is iso-structural to $\beta\text{-Ni}(\text{OH})_2$ -like phase.^[24] Figure 6b is the structural configuration of the $\beta\text{-Ni}(\text{OH})_2$ -like phase, where Ni is replaced by “M” (Ni and Mn), in which the MO_6 octahedral layers stack along the c -axis, while the hydrogen atoms are located between nearby MO_6 octahedral layers.

Cathode materials with various lithium contents were synthesized from precursor #3 with solid state reactions, as described in the experimental section. The nickel-to-manganese atomic ratio is 1:3 based on ICP-MS analysis, exactly matched the nominal ratio. Figure 7 shows SEM images of primary particles with various lithium content. The measured lithium-to-transition metal atomic ratio is indicated in the upper right corner of each image. After lithiation, the primary particles maintain a lamellar morphology, but the edges are much thicker than those of the hydroxide precursors. It was found that, with

the increase of lithium content, the average edge thickness linearly increased from 100 nm for the $\text{Li}_{1.54}\text{Ni}_{0.25}\text{Mn}_{0.75}\text{O}_{2+\delta}$ sample to 500 nm for the $\text{Li}_{1.71}\text{Ni}_{0.25}\text{Mn}_{0.75}\text{O}_{2+\delta}$ sample.

The structure of the cathode materials with varying lithium content was characterized with XRD, as shown in Figure 8(a). The diffraction patterns are similar for different lithium content, with a major phase corresponding to $\text{LiNi}_{0.5}\text{Mn}_{0.5}\text{O}_2$ ($R\bar{3}m$ space group) and a minor phase corresponding to Li_2MnO_3 -like phase ($C2/m$ space group). The right shifting of the (003) peak at $2\theta = 19^\circ$ when lithium content is increased is shown in Figure 8(b) (the 1.67Li sample is an outlier). This slow shift indicates a continuous shrinking of the c-axis lattice parameter. As the direction perpendicular to the c-axis is indicative of lithium ion fast diffusion, the decrease in the inter-planar distance along the c-axis should lead to reduced channel size and, therefore, possible decreased electrochemical performance, as discussed below.

The voltage profiles in the first cycle and capacity retention over 50 cycles are shown for six lithium cells in Figures 9 and 10, respectively. In Figure 9, all the voltage profiles exhibited the typical features of lithium- and manganese-rich composite material: in the charge process, a plateau appears around 4.5 V, which is related to the activation of Li_2MnO_3 -like phase; in the discharge process, a sloped curve rather than a plateau appears due to the concurrence of the reduction of Ni^{4+} and Mn^{4+} to Ni^{2+} and Mn^{3+} , respectively. Compared to lithium-rich composite cathodes made from carbonate precursors ($C_{\text{carbonate}}$) in our previous study,^[4] cathodes based on hydroxide precursors ($C_{\text{hydroxide}}$) have slightly higher initial discharge capacities, and much better tolerance to lithium content variations. For example, an increase of 1.5 to 1.65 Li in $\text{Li}_x\text{Ni}_{0.25}\text{Mn}_{0.75}\text{O}_{2+\delta}$ for $C_{\text{carbonate}}$ can lead to a dramatic capacity decrease from 250 mAh/g

to 125 mAh/g at the C/10 rate in the first discharge; however, as shown in Figure 9, $C_{\text{hydroxide}}$ with a range of 1.54 to 1.67 Li in $\text{Li}_x\text{Ni}_{0.25}\text{Mn}_{0.75}\text{O}_{2+\delta}$ can deliver specific capacities higher than 225 mAh/g at the C/3 rate in the first discharge. As shown in Figure 10, stable discharge capacities higher than 200 mAh/g can be delivered from cathodes with lithium content from 1.54 to 1.71 Li at the C/3 rate (1 C equivalent to 200 mA/g) for the first 50 cycles. Even though the 1.71 Li cathode material delivered a lower discharge capacity in the first several cycles, the specific capacity slowly approached 200 mAh/g after 50 cycles. The performance advantage of the $C_{\text{hydroxide}}$ may arise from the nanoplate morphology of the primary particles, which shorten the lithium diffusion path, and thus facilitate the activation of Li_2MnO_3 -like phase.

Conclusions

Lithium- and manganese-rich cathode materials with excellent electrochemical performance were synthesized via sodium and ammonia hydroxide as the precipitation agents. It was found that ammonia content has a significant effect on both the primary particle size and morphology of agglomerates. When the ammonia concentration was at the higher side, the growth of lamellar primary particles in the lateral direction was promoted, while the thickness of the lamellar primary particles remained at levels less than 50 nm. When the ammonia concentration was at the low side, local concentration of the ammonium-metal ion complex could be too low to sustain effective growth of the particles. Only appropriate ammonia concentrations can promote the lamellar growth in the stacking direction and the effective packing of the primary particles in the agglomerates, which, in turn, enhances the trimming effect provided by effective particle collisions inside the CSTR reactor. As a result, agglomeration with good spherical shape

and high tap density was expected. The Li-and Mn- rich composite cathode materials synthesized based on these hydroxide precursors have a better tolerance to lithium variations compared to those based on carbonate precursors. This superiority in electrochemical performance could be linked to the primary particle morphology control through the ammonia coprecipitation process.

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Figure captions

Figure 1: Average particle size evolution of $\text{Ni}_{0.25}\text{Mn}_{0.75}(\text{OH})_2$ precipitates as a function of reaction time for selected reactions with four M_S/M_A ratios

Figure 2: Particle size distributions of final collected $\text{Ni}_{0.25}\text{Mn}_{0.75}(\text{OH})_2$ precursors for reactions with six M_S/M_A ratios

Figure 3: SEM images of $\text{Ni}_{0.25}\text{Mn}_{0.75}(\text{OH})_2$ secondary particles synthesized with different M_S/M_A ratios in the base solutions: (a) 2:3, (b) 1:1, (c) 3:2, (d) 2:1, (e) 5:2, and (f) 4:1

Figure 4: SEM images of $\text{Ni}_{0.25}\text{Mn}_{0.75}(\text{OH})_2$ primary particles synthesized with different M_S/M_A ratios in the base solutions: (a) 2:3, (b) 1:1, (c) 3:2, (d) 2:1, (e) 5:2, and (f) 4:1

Figure 5: Photos of three filtrated supernatant solutions from precursor-basic solution mixtures with (1) $M_S/M_A = 2:3$, (2) $M_S/M_A = 1:1$, and (3) $M_S/M_A = 4:1$. Two photos on left show NiSO_4 and $[\text{Ni}(\text{NH}_3)_n]^{2+}$ solutions as references

Figure 2: (a) XRD patterns of $\text{Ni}_{0.25}\text{Mn}_{0.75}(\text{OH})_2$ precursors synthesized with different base solutions: 2:3, 1:1, 3:2, 2:1, 5:2, and 4:1. The 2θ Bragg positions for $C2/m$, $I4_1/amd$, and $P\bar{3}m$ phases are drawn together for comparison. (b) Structural configuration of β -Ni(OH)₂-like phase.

Figure 3: SEM images of cathode primary particles with lithium content from 1.54 to 1.71 Li in $\text{Li}_x\text{Ni}_{0.25}\text{Mn}_{0.75}\text{O}_{2+\delta}$

Figure 8: (a) XRD of cathode materials with lithium content from 1.54 to 1.71 Li in $\text{Li}_x\text{Ni}_{0.25}\text{Mn}_{0.75}\text{O}_{2+\delta}$ and (b) zoom-in view of (003) peaks with peak shift highlighted by the black dash line

Figure 4: Voltage profiles in the first cycle with C/10 rate for lithium cells with lithium content from 1.54 to 1.71 Li in $\text{Li}_x\text{Ni}_{0.25}\text{Mn}_{0.75}\text{O}_{2+\delta}$

Figure 10: Cycling performance at C/3 rate of lithium cells with lithium content from 1.54 to 1.71 Li in $\text{Li}_x\text{Ni}_{0.25}\text{Mn}_{0.75}\text{O}_{2+\delta}$

Table captions

Table 1: Experimental conditions for the $\text{Ni}_{0.25}\text{Mn}_{0.75}(\text{OH})_2$ co-precipitation reactions

Figure 1

Figure 2

Figure 3

Figure 4

Figure 5

Figure 6

Figure 7

Figure 8

Figure 9

Figure 10

Table 1

Experiment	T (°C)	Metal sulfate (M)	Control PH	RPM	NaOH/NH ₃ .H ₂ O	Tap density (g/cm ³)
#1	60	2	11	1000	2:3	0.74
#2	60	2	11	1000	1:1	1.5
#3	60	2	11	1000	3:2	0.80
#4	60	2	11	1000	2	0.84
#5	60	2	11	1000	5:2	0.73
#6	60	2	11	1000	4:1	0.54