High-rate axial-field ionization chamber for particle identification of radioactive beams

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Abstract

The design, construction and performance characteristics of a simple axial-field ionization chamber suitable for identifying ions in a radioactive beam are presented. Optimized for use with low-energy radioactive beams (< 5 MeV/A) the detector presents only three $0.5 \mu\text{m}/\text{cm}^2$ foils to the beam in addition to the detector gas. A fast charge sensitive amplifier (CSA) integrated into the detector design is also described. Coupling this fast CSA to the axial field ionization chamber produces an output pulse with a risetime of 60-70 ns and a fall time of 100 ns, making the detector capable of sustaining a relatively high rate and providing a time resolution of 6-8 ns. Tests with an α source establish the detector energy resolution as $\sim 8\%$ for an energy deposit of ~ 3.5 MeV. The energy resolution with beams of 2.5 and 4.0 MeV/A ^{39}K ions and the dependence of the energy resolution on beam intensity is measured. At an instantaneous rate of 3×10^5 ions/s the energy resolution has degraded to 14% with a pileup of 12%. The good energy resolution of this detector at rates up to 3×10^5 ions/s makes it an effective tool in the characterization of low-energy radioactive beams.

Keywords: ionization chamber, particle identification, radioactive beam

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16 1. Introduction

17 The development of radioactive isotope beams (RIBs) has enabled the inves-
18 tigation of nuclei away from β -stability [1–4], which is crucial in understanding
19 nucleosynthesis in exotic astrophysical environments [3], as well as the structure
20 of exotic nuclei [3, 4]. RIBs can be produced by a variety of techniques includ-
21 ing projectile fragmentation [5], ISOL [6], and photofission [7]. As the primary
22 nuclear reaction produces a distribution of product nuclei, to provide a useful
23 secondary radioactive beam, it is necessary to select the nuclide of interest from
24 this distribution. This separation is typically accomplished through electromag-
25 netic means [8]. Often, however, this separation does not produce a pure beam,
26 and other reaction products with similar mass-to-charge ratios contaminate the
27 beam. An effective way to address this challenge is to identify each ion in the
28 beam on a particle-by-particle basis. A commonly used approach to accomplish
29 this is through measurement of the energy loss (ΔE) and time-of-flight (TOF)
30 of each ion [9].

31 The ΔE information is often obtained from gas ionization chambers [10]
32 used in transmission mode. The uniform thickness achievable with these de-
33 tectors, as well as their robustness against radiation damage are key factors in
34 their utility. A common geometry of an ion chamber utilizes an electric field
35 transverse to the incident ion direction [11], with a Frisch grid used to remove
36 the dependence of the pulse amplitude on position. In this geometry of ion
37 chambers, however, the drift time of the electrons in the direction transverse to
38 the beam direction typically limits the rate to $\sim 10^4$ ions/s. To overcome this
39 limitation of a slow response time, an axial field design can be employed. Ax-
40 ial field ionization chambers have been successfully employed as ΔE detectors
41 for heavy-ions since the 1980's [12, 13]. Recently, the high rate capability of
42 this design has been exploited at both high [14] and low energies [15] by using
43 multiple tilted electrodes in the beam path to identify reaction products in a
44 radioactive beam. When the incident energy is sufficiently high (~ 100 MeV/A)
45 thin metallized foils have been utilized for the electrodes. In contrast, at low

Figure 1: CAD drawing of the Rare Ion Purity Detector in an exploded view. A: window frame. B: anode ring. C: PCB. D: RIPD. body E: window frame. The mylar windows and central anode foil are omitted for clarity.

incident energies (~ 5 MeV/A) the electrodes consist of wire harps. Both designs involve the insertion of multiple electrode planes (15-24) into the beam path, a source of considerable scattering and energy loss for the incident ion. In the subsequent sections, we describe the development and characterization of a simple high-rate axial-field ionization chamber, designated the Rare Ion Purity Detector (RIPD) which inserts a minimal amount of material into the beam path. The compact, minimalist design of this detector is capable of operating at a rate only slightly less (3×10^5 pps) than that of the more complex, tilted multi-electrode geometry (7×10^5 pps) [15] while presenting a minimal source of additional scattering of the incident beam.

2. Physical Configuration

The principal motivation in developing this detector was investigation of fusion for neutron-rich light ion beams at energies near the fusion barrier [16, 17]. Due to the low energy beams utilized in these experiments, particular attention was given to the total thickness of the detector in order to minimize the beam divergence and energy straggling incurred by inserting the detector into the

beam path. Prior experience established that minimizing scattering of the beam was essential. This requirement meant eliminating any wire planes in the beam path. To implement the simplest axial field geometry while minimizing the electron collection time, a central anode is used with the metallized windows serving as cathodes.

A CAD drawing of RIPD is shown in Fig. 1. The detector is comprised of an aluminum body, two stainless steel window plates, and a thin central anode foil. The anode is coupled to a charge sensitive amplifier (CSA) housed inside the aluminum body. The body measures approximately 11 cm x 11 cm transverse to the beam direction and 2.0 cm thick along the beam axis. The window plates are 5 mm thick and have a 38 mm diameter opening for the beam to pass through, over which 0.5 μm aluminized mylar is epoxied. These mylar foils serve to contain the gas within the active volume and act as cathodes. The window plates are sealed to the body of the detector using O-rings. No support wires are used with these windows to minimize scattering of the incident beam. Using this geometry, it is possible to operate the detector at a pressure of 30 torr of CF_4 for several days without any noticeable degradation in the window performance. Repeatedly filling the detector with gas also did not cause a noticeable deterioration in the mylar window. The 0.5 μm mylar anode foil, which is doubly aluminized, is mounted on a 2.0 cm diameter stainless steel ring. This ring is attached to an annular printed circuit board (PCB) with an inner diameter of 2.0 cm and an outer diameter of 7.4 cm. The position of the PCB is chosen so that the distance between the anode foil and each cathode foil is 1 cm. Holes in the PCB allow gas to flow between the two halves of the detector. This arrangement of the anode and CSA in close proximity minimizes any additional capacitance at the input of the CSA.

3. Charge Sensitive Amplifier

As a key goal in the design of this axial field ionization chamber is its ability to maintain good energy resolution while sustaining a high rate with minimum pileup of signals, it was necessary to develop a fast, low-noise charge

Figure 2: Schematic of the charge sensitive amplifier for RIPD.

sensitive amplifier. Ionization of the detector gas induced by a beam particle traversing RIPD quasi-instantaneously produces an ionization track in the detector. Electrons in this track migrate under the influence of the applied electric field and are collected at the central anode. It should be noted that in contrast to the tilted foil design [14, 15] the electric field in RIPD does not move the electrons away from the path of the ionizing beam. Thus, in comparison to the tilted foil geometry the effects of recombination and screening are expected to be larger. This disadvantage is offset by the simplicity of the present design. Carbon tetrafluoride (CF_4) was chosen as the detector gas due to its high electron drift velocity [18]. Based upon the electron drift velocity for a reduced field of $1 \text{ kV cm}^{-1} \text{ atm}^{-1}$, a rise time of 100 ns is anticipated. This charge collection time defined one of the necessary characteristics of the CSA. To minimize the impact of stray capacitance, the CSA was situated on the PCB as close as practically possible to the central anode. The input capacitance of the detector was calculated to be 2.25 pF, which was confirmed by measurement.

The CSA is a new design that is intended to enable high count rates from low capacitance detectors. The design was initially intended to resolve beam contaminants arriving simultaneously with multiple beam ions in a 12nS interval. Achieving this separation required a bandwidth exceeding 80MHz. With a feedback resistor of 18 k Ω , a bandwidth of 90 to 100 MHz was achieved. Changes in the experimental requirements led us to increase the gain of the CSA, consequently decreasing the bandwidth, by increasing the feedback resistor value. The schematic of the CSA is shown in Fig.2. The first opamp (U1) provides most of the gain with only a small contribution to the overall noise. However, its bias current, input current noise, and input capacitance are too high for direct connection to the anode, so a SiGe microwave transistor (Q1) is added to serve as an input buffer. This particular transistor offers very high current gain (about 2000) and extremely low input capacitance, and is also very quiet. Choice of a JFET for this purpose was precluded by the bandwidth originally intended. The signal response of this composite amplifier is defined by the feedback network of R69 and C7, 8, and 9. R69 is actually 4 chip resistors totaling

Figure 3: Cross-sectional view of the experimental setup to measure the energy loss of α particles. An ^{241}Am α source was placed just upstream of the entrance foil in a cap that was made common with the active volume. Alpha particles that pass through the full length of the detector were then measured in a silicon surface barrier detector (SBD) placed just downstream of the exit window in a cap that was also made common with the active volume. A: ^{241}Am α source. B: Entrance cathode foil. C: Anode foil. D: CSA. E: Exit cathode foil. F: SBD.

123 800 kohms, which were stacked end to end to minimize stray capacitance. The
 124 capacitors form a network with an equivalent capacitance adjustable from 0.1
 125 to 0.3 pF. This network simplifies to just a RC single-pole response. The anode
 126 board also comprises an output buffer with a gain of 2, two voltage regulators
 127 (U4 is remarkably low noise), level shift, and anode bias circuits. Minimizing
 128 the size of the circuit was dictated by the need to minimize parasitics. This
 129 circuit was realized on a annular FR4 printed circuit board on which the RIPD
 130 anode was mounted. Excluding the bias and power circuit the CSA occupies an
 131 area of approximately 19 mm x 19 mm. At 12V the circuit consumes 24ma.

132 4. Experimental setup

133 To characterize the performance of RIPD, the energy resolution for α parti-
 134 cles from an ^{241}Am source was measured. To test RIPD with α particles, which
 135 have a low ionization density, it is necessary to operate RIPD at gas pressures

136 that exceed the maximum pressure sustainable with the thin windows. For these
 137 tests, the entrance and exit window plates were replaced with flanges, as shown
 138 in Fig 3. The entrance flange allowed an ^{241}Am source to be situated prior to
 139 the entrance cathode foil but within the gas volume. Correspondingly, the exit
 140 flange allowed a silicon surface barrier detector (SBD) to be placed after the
 141 exit cathode foil within the gas volume. Both the ^{241}Am source and SBD had a
 142 collimation of 3 mm. Triggering on the SBD signal associated with arrival of α
 143 particles selected particles that had traversed the entire thickness of RIPD. Us-
 144 ing this configuration, signals in RIPD could be examined for pressures between
 145 100 and 400 torr. At a pressure of 100 torr the 5.48 MeV α particles deposit
 146 just 680 keV in the gas. This energy deposit increases to ~ 3.5 MeV at 400 torr.

147 5. Signals

148 A typical signal from the CSA at a pressure of 300 torr is shown in Fig. 4.
 149 The anode was biased to a potential of +395 V to produce a reduced field of 1
 150 $\text{kV cm}^{-1} \text{ atm}^{-1}$. The signal time from baseline to peak is approximately 100 ns
 151 with a rise time of 60 ns. Although the observed signal rise time corresponds to
 152 the convolution of the electron collection time and the CSA response, as the CSA
 153 response is fast (< 10 ns), the observed signal principally reflects the electron
 154 collection time, consistent with the reported literature value for the electron
 155 drift velocity at the reduced field utilized. The CSA signal returns to baseline
 156 after 300 ns. Thus the whole signal duration is under 500 ns, which corresponds
 157 to a maximum calculated rate of $\sim 2 \times 10^6$ ions/second without pileup. The
 158 gain of the CSA is approximately 9.5 mV/MeV. The noise of this signal is
 159 approximately 4 mV peak-to-peak, corresponding to a signal-to-noise ratio of
 160 5.7.

161 To handle these fast signals, the development of a fast shaping amplifier
 162 was required. This requirement was realized by modifying an in-house octal
 163 shaper module which handles input signals of both polarities. With the fast
 164 shaper module shaping times between 100 ns and 800 ns in increments of 100 ns
 165 can be selected. The coarse gain is controlled by two 4-bit stages, while a fine

Figure 4: Typical signal from the CSA corresponding to the energy loss of an ^{241}Am α particle with 300 torr of CF_4 gas in the detector.

gain adjustment is provided using a 12-bit multiplying ADC. Another 12-bit multiplying ADC allows adjustment of the pole-zero. All of these parameters can be adjusted under computer control through a USB 2.0 interface. With a shaping time of 200 ns the fast shaping amplifier transforms the typical input CSA signal depicted in Fig.4 into a Gaussian-like pulse shown with an amplitude of ~ 950 mV and a peak-to-peak high frequency noise of ~ 30 mV. Thus the shaping amplifier improves the signal-to-noise ratio to a value of approximately 31.

6. Energy Resolution

To determine the energy resolution of RIPD, the signal from the shaping amplifier was digitized by a CAEN V785 peak-sensing ADC. The energies of particles measured in RIPD was first calibrated using the measured energies in the SBD detector after accounting for the energy lost in the mylar foils [19]. The calibrated RIPD energy spectrum was used to determine the energy resolution by comparing the FWHM of the energy distribution to its centroid. The dependence of the energy resolution on the energy deposited in the gas volume is shown in Fig. 5. For energies up to ~ 2 MeV, the absolute resolution is constant

Figure 5: Resolution as a function of energy deposit in the gas volume of RIPD for α particles from a ^{241}Am source.

Figure 6: CAD representation of the experimental setup used to characterize RIPD with beam.

183 at a value of approximately 220 keV, suggesting that for these energy deposits
 184 the electronic noise dominates the total noise. Above 2 MeV the absolute resolu-
 185 tion deteriorates reaching a value of ~ 260 keV at 3.5 MeV of energy deposit. In
 186 the energy deposit interval measured the relative resolution decreases smoothly
 187 from 32% to $\sim 7.5\%$. This 7.5% resolution can be understood as a combination
 188 of the signal-to-noise after the fast shaper as well as the variations in the path
 189 length of the measured α particles through the gas volume.

190 **7. Performance with Beam**

191 In order to characterize the performance of RIPD with beams of different
 192 intensity a test was conducted at the ReA3 facility at Michigan State Univer-
 193 sity's National Superconducting Cyclotron Laboratory (NSCL). The ReA3 80
 194 MHz linac, which can be used to accelerate either stable beams or radioactive
 195 ions produced by the NSCL's coupled cyclotron facility, was used to accelerate
 196 ^{39}K to energies of 2.5 MeV/A and 4 MeV/A. The beam was extracted from the
 197 charge breeding ion trap EBIT within 100 milliseconds at a repetition rate of
 198 2 Hz. This time structure results in the instantaneous rate experienced by any
 199 detector in the beam path being effectively a factor of five higher than the av-
 200 erage rate. The experimental setup used is depicted in Fig. 6. The first element
 201 of the setup was a microchannel plate detector [20]. In this detector, passage
 202 of a beam particle through a $100\text{ }\mu\text{g}/\text{cm}^2$ carbon foil ejects electrons that are
 203 transported by crossed electric and magnetic fields to the surface of a chevron
 204 microchannel plate (MCP). The fast response of the MCP results in each beam
 205 ion incident on the carbon foil being individually recorded. The rate at which
 206 the MCP triggers was recorded by a 250 MHz VME scaler providing a measure
 207 of the beam rate. Approximately 44 cm downstream of the MCP, RIPD was
 208 mounted on a retractable arm. For low intensity beams a SBD situated imme-
 209 diately after RIPD was used to measure the residual energy of ions traversing
 210 RIPD. The SBD was retracted from the beam path when a high intensity beam
 211 was used.

Figure 7: Panel a: Dependence of the energy resolution on the deposited energy in RIPD. Panel b: Impact on energy resolution of increased instantaneous beam rate.

Shown in Fig. 7a as the closed triangles is the energy resolution of the energy deposited in RIPD by 2.5 MeV/A ^{39}K ions traversing RIPD at nominal gas pressures of 5, 10, 15, and 20 torr. The gas pressure and flow through the detector were maintained by a high quality gas handling system with a stability of 0.2 torr. With increasing gas pressure the energy deposit in the gas increases from approximately 1 MeV to approximately 5 MeV. As the energy deposit in the gas increases the relative resolution of RIPD improves from 25% at the lowest energy deposit to approximately 9% at the highest energy deposit in reasonable agreement with the source testing results presented in Fig. 5. The electronic noise as well as the stability of the electronics were monitored during the measurement by injecting a calibration pulse into the charge sensitive amplifier at a low rate. The electronic noise was measured to be approximately 1 %, significantly less than the measured energy resolution of the detector. To determine the response of the energy resolution of RIPD to a change in the beam intensity, the beam intensity of a 4 MeV/A ^{39}K beam was increased from 800 ions/s to 3×10^5 ions/s. The impact of the beam intensity on the energy resolution of RIPD is shown in Fig. 7b. With increasing beam intensity the measured energy resolution degrades from approximately 9% to $\sim 14\%$ at the highest intensity measured.

Figure 8: Impact of the beam intensity on the charge collection (panel a) and pileup (panel b) in RIPD.

231 Aside from the degradation in the energy resolution the increased beam
 232 intensity can also impact the total charge collection due to increased recom-
 233 bination in the detector at high beam intensities. This effect is manifested in
 234 the upper panel of Fig. 8. A decrease in the centroid of the energy deposited
 235 in RIPD by 4 MeV/A ^{39}K ions is evident. With increasing beam intensity the
 236 location of the energy centroid shifts to lower values consistent with recomb-
 237 ination of electrons and cations in the detector gas. At an instantaneous rate
 238 of 3×10^5 ions/s a peak shift of $\sim 12\%$ is observed as compared to a low in-
 239 tensity beam of 800 ions/s. As recombination impacts both the ions of interest
 240 as well as any contaminants, identifying the nuclide of primary interest from
 241 other contaminants is still achievable. However, correcting for any significant
 242 changes in the beam intensity becomes important. For the secondary beams
 243 that are the principal focus of this detector the beam is often extracted from
 244 a charge breeder prior to reacceleration leading to a macro time structure of
 245 the beam. Within this extraction pulse the instantaneous beam intensity will
 246 typically vary. By recording the extraction time within the extraction cycle
 247 into the data stream this variation in the instantaneous rate can be accounted
 248 for.

249 The impact of beam intensity on the pileup observed is indicated in the
 250 lower panel of Fig. 8. Pileup is clearly distinguished as observation of pulses
 251 with energies exceeding that of the full beam energy. As expected the pileup
 252 increases with increasing instantaneous rate from $<1\%$ at 1×10^4 ions/s to just
 253 under 12% at 3×10^5 ions/s. As anticipated the fast response of RIPD enables
 254 the use of the detector at high rates without significant pileup.

255 We have also assessed the time resolution of RIPD by measuring the ΔE -
 256 TOF of the beam. The TOF was measured between RIPD and the MCP de-
 257 tector. Due to the sub-nanosecond time resolution of the MCP detector the
 258 measured time resolution is dominated by the time resolution of RIPD. The
 259 CSA signal was amplified with a timing filter amplifier with integration and dif-
 260 ferentiation times of 40 and 20 ns respectively prior to discrimination. The
 261 TOF between the MCP and RIPD was measured using a CAEN V1290 TDC

with a resolution of 25 ps. At beam intensities of $<1 \times 10^3$ ions/s for an energy deposit of approximately 5.4 MeV a time resolution of 6.8 ns (FWHM) is obtained. With increasing beam intensity this resolution degrades slightly to 8 ns. For smaller energy deposits in the gas the resolution worsens reaching a time resolution of 13.2 ns for an energy deposit of 2.3 MeV. This time resolution is remarkably good for an ionization chamber and is consistent with the inherently fast risetime and good signal-to-noise evident in Fig.4. This time resolution could be useful in complex multidetector systems as a means to remove pileup events.

8. Conclusion

To address the challenge of identifying contaminant species in radioactive isotope beams, we have developed a high-rate axial-field ionization chamber which introduces minimal material into the beam path. The high-rate capability of this detector was optimized by implementing a low profile central anode design and developing a fast charge-sensitive amplifier which is situated within the gas volume in close proximity to the anode. A typical signal from this amplifier spans less than 500 ns, with a rise time of approximately 60-70 ns. The fast response of this detector results in a typical time resolution of 6-8 ns making its timing useful for random/pileup rejection. A fast shaping amplifier was developed to handle these fast signals. With these pulse shaping electronics the energy resolution of RIPD is approximately 8% for an energy deposit of 3.5 MeV in the detector for α particles from an ^{241}Am source. Using beam, a comparable resolution was obtained. Below an instantaneous rate of 1×10^5 ^{39}K ions/s the energy resolution was 8-10%. At an instantaneous rate of 3×10^5 the energy resolution degraded to 14%. The impact of recombination and pileup in the detector as a function of the instantaneous rate was characterized. Correcting for these effects is an important part of exploiting the full capability of this detector to resolve contaminants in a radioactive beam.

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