MCViNE – An object oriented Monte Carlo neutron ray tracing simulation package

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Abstract

MCViNE (Monte-Carlo Virtual Neutron Experiment) is an open-source Monte Carlo (MC) neutron ray-tracing software for performing computer modeling and simulations that mirror real neutron scattering experiments. We exploited the close similarity between how instrument components are designed and operated and how such components can be modeled in software. For example we used object oriented programming concepts for representing neutron scatterers and detector systems, and recursive algorithms for implementing multiple scattering. Combining these features together in MCViNE allows one to handle sophisticated neutron scattering problems in modern instruments, including, for example, neutron detection by complex detector systems, and single and multiple scattering events in a variety of samples and sample environments. In addition, MCViNE can use simulation components from linear-chain-based MC ray tracing packages which facilitates porting instrument models from those codes. Furthermore it allows for components written solely in Python, which expedites prototyping of new components. These developments have enabled detailed simulations of neutron scattering experiments, with non-trivial samples, for time-of-flight inelastic instruments at the Spallation Neutron Source.

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Examples of such simulations for powder and single-crystal samples with various scattering kernels, including kernels for phonon and magnon scattering, are presented. With simulations that closely reproduce experimental results, scattering mechanisms can be turned on and off to determine how they contribute to the measured scattering intensities, improving our understanding of the underlying physics.

Keywords: neutron scattering, Monte Carlo simulation, ray-tracing, inelastic, spectrometry

1. Introduction

Data analysis for neutron time-of-flight spectroscopy has predominantly been a conversion of raw data to intensities with instrument independent units; namely $S(\mathbf{Q}, \omega)$ or $S(\mathbf{Q}, E)$, where S is the dynamical structure factor, and
5 $\mathbf{Q}$, ω , E are the wave vector, frequency, and energy. This approach has been the basis for many studies, but some cases require a more elaborate analysis scheme (see, for example, [1, 2, 3, 4, 5, 6, 7, 8, 9]).

More specifically, traditional reduction assumes single scattering, that the resolution function can be modeled by a simple function, that the scattering
10 process of interest can be readily separated from other scattering processes in the system, and that scattering from the sample environment is negligible or easily subtracted. Monte Carlo ray-tracing can provide a straightforward way to perform analysis in cases where some, or all, of the above assumptions are not valid. Specifically it can be used to investigate complex samples whether
15 they have multiple scattering, multiple modes of scattering, i.e. magnetic and lattice vibrations, or consist of a conglomeration of scatterers like a sample and sample environment. Additionally as the instrument is modeled component by component, instrument resolution is inherently included in the simulation.

As the promise of Monte Carlo ray tracing was clear, it has been used in
20 codes that handle a subset of these complexities. MCS[10] and MSCAT[11] were early packages that used Monte Carlo methods to compute multiple scattering.

Later, several general-purpose Monte Carlo neutron instrument simulation packages were developed and optimized to help design neutron instruments, namely McStas [12, 13], VITESS [14], IDEAS [15], and NISP [16]. Less-general-purpose
25 MC programs exist in some popular neutron data analysis software packages, including DISCUS [17, 18, 19] and RESTRAX [20, 21]. In comparison, relatively few studies [22, 23, 24, 25, 26] have employed full-fledged Monte Carlo ray tracing to help analyze experimental results from neutron scattering measurements, while there are growing efforts to perform virtual neutron experiments using
30 MC ray tracing [27, 28, 29, 30, 31]. MCViNE[32], an open source software, is designed to easily allow complex studies (see [9] for an example) and therefore should accelerate the use of Monte Carlo ray tracing in the analysis of experimental data.

The improvements in computing over the last decades include hardware de-
35 velopments, the emergence of object-oriented languages C++ and Python, and advances in software design [33]. The amazing increases in hardware capabilities now allows detailed simulations to run in a reasonable time. The impact of modern software engineering practice on MC simulation codes is still progressing. MCViNE was developed, as part of the DANSE project [34], using such soft-
40 ware practices. Therefore it uses object oriented programming (OOP) concepts to represent instrument and sample components, following the hierarchical and modular nature of the neutron instruments, detector systems, and sample environments. This use of hierarchies from inside an instrument component or sample kernel up through the total instrument goes beyond the imperative pro-
45 gramming paradigm, which is popular in other codes.¹ By taking advantage of OOP design patterns as well as recursive algorithms, the MCViNE architecture supports an easily extensible library for scattering kernels suitable for both samples and detector systems. This approach allows for maximum flexibility, extensibility, and reuse of scatterer arrangements, geometrical shapes, and
50 scattering mechanisms, and hence improves the sustainability of the software.

¹A brief discussion is available in the supplemental material.

This paper contains a description of the MCViNE software framework. Section 2 presents the challenges in simulating experiments carried out in modern neutron instrumentation, and an overview of the software engineering design and main software components and algorithms. Examples of MCViNE simulations for powder and single-crystal experiments are presented in Section 3. Concluding remarks follow in Section 4.

2. Simulation of Spectra Measured at Modern Neutron Spectrometers with MCViNE

2.1. Challenges for simulating neutron scattering experiments

Monte Carlo (MC) ray tracing simulations of neutron scattering spectrometers with support of multiple scattering were performed from 1970s using MCS[10] and MSCAT[11]. They were used to understand the effects of multiple scattering on the measured spectra [35]. In the 1990s, with increasing needs of simulating neutron instruments for the purpose of instrument design and optimization, several MC neutron ray tracing packages emerged, including McStas[12, 13], Vitess[14], Ideas[15], and NISP [16]. Simulations performed with these packages provide not only independent checks for analytical calculations of instrument performance, but also can be used to obtain optimal parameters for instrument design (see, for example, [36, 37, 38, 39, 40, 41, 42, 43, 44, 45]). Unlike MCS and MSCAT, most of these newer MC software packages (with a notable exception in NISP) treat simulation of a neutron instrument as a linear chain of neutron optical components, each of which modify some set of neutron beam characteristics such as spatial divergence and energy distribution. This linear approach greatly improved the computational efficiency and simplified the coding of instrument simulations. Such an approach is adequate because the physical formation of a neutron scattering instrument is linear, and the underlying hypothesis that neutrons at the downstream components are rarely scattered back to the upstream components holds up well in most instrument

configurations. As a result, these software packages, especially McStas and
80 Vitess, are making significant impacts for neutron instrument design.

For Monte Carlo neutron ray tracing simulations to be useful for interpretation of neutron scattering spectra, it is necessary to include detector systems and samples/sample environments, for which the physical arrangements are often non-linear. The detector systems in modern neutron scattering instrumen-
85 tation display modularity, repetition, and sometimes hierarchical organization, reducing the engineering difficulties in manufacturing, testing, and validation. For example, the four direct geometry time-of-flight spectrometers at Spallation Neutron Source (SNS) [46], ARCS [47], SEQUOIA [48, 49], CNCS[50], and HYSPEC[51] share some instrument elements[52]: the Fermi chopper slit pack-
90 ages for the ARCS and SEQUOIA instruments are interchangeable, and the detector systems of all four instruments use the same so-called 8-packs [53], each of which is a detector pack consisting of eight ^3He linear position sensitive detector tubes (LPSD). The 8-packs are arranged in a vertically-oriented cylindrical geometry around the sample position, forming a hierarchical orga-
95 nization of pixels, tubes, packs, and detector rows. A simplified illustration of the detector hierarchy can be found in Figure 1(c).

Samples, sample holders, and sample environments are constituents of a “sample assembly”, the term we use to refer to the collection of neutron scatterers near the sample position. A sample-assembly example is illustrated in
100 Figure 1(b). A linear representation faces challenges in simulations of a sample assembly because it does not match physical arrangements of a sample or samples with associated sample environment components, and because neutrons can often scatter back and forth among the constituents. A good example of complex sample environments is the MICAS furnace [54]: the incident neutron
105 beam intersects heating elements and up to 8 heat shields, all thin vertical hollow cylinders, in addition to the sample. The sample itself can be challenging too. For example, “single crystal” superconductor samples for inelastic neutron scattering experiments often consist of co-aligned arrays of small crystals mounted on an aluminum plate [55]. Another major difficulty stems from the

110 fact that a variety of different scattering mechanisms may be present in the
combination of sample, sample holder, and sample environment.

2.2. General capabilities of MCViNE

MCViNE[32] is a general purpose neutron ray tracing package that combines
the two different approaches taken by MSCAT-like packages and McStas-like
115 packages. At the instrument level, it allows users to create a simulation appli-
cation as a linear chain of neutron components, each fully configurable by its
type and corresponding geometrical and physical properties using either com-
mand line options or an xml-based configuration file. At the component level,
two general components exist with support of hierarchical representation for the
120 sample assembly and the detector system. A detector system can be specified
with an xml file describing its hierarchy, while a sample assembly is specified by
a collection of xml files, one for the geometrical organization of the constituent
scatterers, and others describing the scattering mechanisms for them. Multiple-
scattering among scatterers in a sample assembly can be turned on and off by
125 a command line option.

2.3. Architecture Overview

MCViNE is implemented in C++ and Python. The C++ portion contains
fundamental mathematics, the neutron ray tracing mechanism, the mechanism
to include components from other MC ray tracing packages, and support of
130 multiple scattering and composite scattering kernels. These various functions
of the C++ code are implemented in two layers, which are discussed in the
supplementary information. There are two aspects of the C++ usage that
bear more discussion. The components from McStas are included in the C++
layer so that they can be used as individuals rather than as a whole compiled
135 instrument. Also, the combination of the object oriented features of C++ and
the speed of the compiled code make this the appropriate place to implement the
composite kernel and scattering kernels. Currently two such components exist,

Figure 1: Concepts in scattering composites: composite scatterer, homogeneous scatterer, shape, scattering kernels. (a) an abstract hierarchy of an arbitrary scattering composite. (b) and (c) are concrete examples of such hierarchies. (b) top view of a sample assembly consisting of an aluminum can and a copper plate. (c) a detector system – how it is constructed from an elemental scatterer (detector tube) in a three-level hierarchy.

one for sample assemblies and one for detector systems. This unique feature of MCViNE, the “composite scatterer”, will be explained in detail in section 2.4.

140 A Python layer on top of the two C++ layers allows construction of a component chain similar to McStas-like neutron ray tracing packages, provides the interface to the C++ components to include in that chain, and allows for introduction of components that are completely written in Python. This last feature makes it extremely easy to create simple neutron components, and to create

145 prototypes of more sophisticated neutron components.

2.4. Composite Scatterer

This section starts with basic concepts with regard to the “composite scatterer”, followed by an introduction to the essential object-oriented software designs centered around it, and finishes with examples of ray-tracing algorithms in sample assemblies and detector systems, enabled by these designs and needed in simulation of neutron scattering experiments in modern spectrometers.

2.4.1. Concepts

In MCViNE, a “composite neutron scatterer” represents a group of physical objects, for example, a powder sample in an aluminum can, a single crystal sample surrounded by a furnace, or a detector system. An “elemental scatterer” is a scatterer without constituent scatterers. A “homogeneous scatterer” is one kind of elemental neutron scatterer, whose scattering function is homogeneous within its volume. The scattering properties are modeled using one “scattering kernel” or a combination of several “scattering kernels”, each of which represents one scattering mechanism, such as incoherent one-phonon nuclear scattering or coherent magnetic scattering.

These concepts are illustrated in Figure 1. Figure 1(a) is an example of an abstract hierarchy of a composite scatterer in MCViNE. In principle, the hierarchy in MCViNE can be arbitrarily deep. In practice, the depth of the hierarchy is limited by factors such as computing resources available for the simulations, and compiler limitations. Figure 1(b) depicts a sample assembly that is a composite of two-level hierarchy, in which the bottom level consists of two homogeneous elemental scatterers: one aluminum can and one copper plate sample. Figure 1(c) represents a detector system consisting of ^3He eight-packs that form roughly a cylindrical arrangement around the sample position. The detector system is represented in MCViNE in a three-level hierarchy: at the bottom level is the ^3He detector tube; at the middle level, 8 such tubes construct an 8-pack; at the top-level, the detector system consists of a collection of 8-packs. Such hierarchical representations allow MCViNE to model the physical reality closely.

2.4.2. Object Oriented Designs

These concepts lead to one major design decision made in the MCViNE project: employment of the “composite design pattern”, which is used to describe the part-whole relationship and to represent a hierarchy, and allows clients
180 to treat composites and their constituents in a uniform way, and the “visitor design pattern”, which allows separation of operations from the objects to be operated on, so that new operations can be added without touching these objects [33]. By using these design patterns for scattering composites, we can unify the programming interfaces to the operations on both the composites and the
185 individual elemental objects. Composite and visitor patterns are used in three major aspects of the MCViNE neutron scattering model: the neutron scatterers, the geometric shapes of scatterers, and the scattering kernels.

Neutron scatterers. By using the composite pattern, algorithms for multiple scattering can be consolidated in one implementation. Scattering from a
190 composite neutron scatterer starts with a determination of which constituent intersects the incident neutron ray, and then delegates the scattering assessment to that particular constituent, which could be a composite itself that requires another delegation for scattering. The hierarchical representation of neutron scatterers and this recursive algorithm work for both samples and detector sys-
195 tems, and can improve computing efficiency and code maintenance.

Geometric shapes Using constructive solid geometry (CSG) (see for example [56]), composite shapes are constructed from basic shapes such as cylinders and blocks, and composites by using operations such as union, intersection and difference. Ray-tracing through shapes is therefore simplified as visitor methods
200 of the primitive shapes and the binary shape operations.

Scattering kernels Composite scattering kernels make it easy for the Monte Carlo algorithm to sample a total $S(\mathbf{Q}, \omega)$ consisting of both slowly-varying regions and regions containing sharp features, such as diffraction and coherent phonon scattering, by allowing users to combine different kernels such as in-
205 coherent and coherent kernels in a kernel composite. In addition, users can

organize scattering kernels into groups; this makes it easy to apply importance sampling (assign different weights to different kernels or kernel groups) in simulations.

A “scattering kernel” in MCViNE is conceptually different from sample components in linear MC neutron ray tracing packages. A scattering kernel in MCViNE is an abstraction of the scattering mechanisms such as diffraction, nuclear scattering by phonons, and magnetic scattering by spin waves. It does not include the sample geometry but only the scattering physics. A sample component in earlier packages, on the other hand, includes both the geometry and the physics in one programming unit. By separating the implementation of “scatterer”, “shape”, and “scattering kernel”, a sample in MCViNE can consist of a combination of scattering kernels. Furthermore, the scattering kernel library in the MCViNE framework can be extended without affecting the logic of geometric ray tracing, which is implemented in “shape” and “scatterer”. For example, for isotropic scattering, scattering kernels taking a histogram form of $S(Q, \omega)$ can be supported, as well as phonon scattering kernels taking phonon energies and polarizations as inputs (examples are given in Section 3.1 and 3.2). A scattering kernel conveniently taking the analytical form of a dispersion can be used (see [9] for an example) to improve convergence (effective when combined with other scattering kernels), and to avoid unnecessary broadenings resulted from approximating $S(Q, \omega)$ using a histogram. Inelastic and elastic scattering kernels for single crystals can also be developed to simulate single crystal experiments.

2.4.3. Algorithms

In this section, the general ray tracing procedure is first described briefly, and then implementation of multiple scattering and ray tracing in detector systems are presented as algorithm examples that benefit from the conceptual analysis and the software design.

Ray Tracing

In components such as sample assemblies or detector systems, neutron scat-

Figure 2: An example of multiple scattering within one scatterer. The incident neutron was scattered three times by three different scattering kernels. At each scattering point, the original neutron is also propagated out of the scatterer with proper attenuation. Red arrows are paths of neutron propagation. Circles highlight the location of scattering. Different scattering events are coded using different colors.

terers are represented by a hierarchy of objects with shapes and scattering mechanisms. Ray tracing of a neutron happens by first investigating which one of the neutron scatterers at the top level of the scatterer composite hierarchy intercepts the neutron. This is done by computing the intersections of the forward ray of the neutron and all the shapes of the top level constituents. A random selection might be necessary if multiple top-level objects intercept the neutron. After the top-level neutron scatterer is identified, the neutron is propagated to the front surface of the scatterer if necessary (not necessary if the neutron is already inside the scatterer) with appropriate attenuation, and then the ray tracing algorithm recurses into itself if the scatterer is a composite. Otherwise a point in the forward path of the neutron inside the scatterer will be randomly picked, and the neutron is propagated to that point with attenuation. At this point a scattering (or an absorption) mechanism of the scatterer is randomly picked, and the neutron will be either scattered with its probability adjusted, or be absorbed.

Multiple Scattering

Multiple-scattering (MS) is naturally supported in MCViNE scattering composites, implemented with a recursive algorithm. For the purpose of this discussion, we differentiate between two types of multiple scattering: single-scatterer

Figure 3: An example of multiple scattering in a concentric sample assembly. Five (out of infinite) possible multiple scattering paths are illustrated.

multiple scattering (SSMS) to describe the multiple scattering within one neutron scatterer and multiple-scatterer multiple scattering (MSMS) to describe multiple scattering among neutron scatterers.

Figure 2 shows an example of SSMS in which a neutron gets scattered three times before exiting a scatterer. Each time a neutron is scattered inside a homogeneous scatterer, the original incident neutron packet is split into two neutron packets for computational efficiency. One neutron packet is propagated through the scatterer with its probability lowered by attenuation, while the other is scattered by one of the scattering kernels, chosen by a random selection, at a point also randomly selected along the forward path of the incident neutron. This splitting process repeats for the scattered neutron several times, as illustrated in Figure 2, until either the neutron probability is lower than a pre-selected limit, or the maximum order of multiple scattering is reached. At this point, the neutron that is still inside the scatterer is allowed to propagate out, with its probability attenuated appropriately.

Figure 3 shows an example of multiple scattering in a sample assembly consisting of a “concentric” arrangement of a sample and a sample environment. Only five of an infinite number of possible multiple scattering paths are illustrated, and the splitting processes are not shown.

The multiple scattering algorithm of MCViNE is generic, and it can handle

275 more complex sample assemblies, such as non-concentric arrangements, and
mixing of non-concentric and concentric arrangements. More details about the
MS algorithm of MCViNE can be found in the supplemental material for this
paper.

Sample components in some linear-chain-based MC ray tracing packages can
280 support SSMS, but they do not have abstractions similar to composite scatterer
or scattering kernel. As a result, the SSMS algorithm must be duplicated in
these sample components, while in MCViNE, implementations of new scattering
kernels can be added without reimplementing the multiple scattering algorithm.
McStas supports MSMS partially for a concentric sample assembly by, for ex-
285 ample, adding a second outer cylinder into the simulation component chain [57].
Path (e) of Figure 3 is included this way, but path (c) of Figure 3 is not. Other
ways of simulating MSMS may be possible with McStas, but these would require
significantly more effort on the user's part.

The multiple scattering algorithm of MCViNE is more comparable to that
290 of MSCAT[11] in which the sample and the sample environment are treated
together in the multiple scattering loop, offering complete treatment of SSMS
and MSMS. However, MCViNE allows a straightforward increase in complexity
of the sample and sample environment interactions by using the recursive MS
algorithm enabled by OOP. MSCAT by default only allows for a few specific
295 arrangements. MSCAT and some McStas components contain the ability to
appropriately transform the angular scattered distribution off of the sample so
as to only simulate neutrons that will impact the detector, such optimization is
not yet available in MCViNE.

Ray tracing in a detector system

300 Ray tracing of a neutron through a sophisticated detector system in instru-
ments such as ARCS and SEQUOIA, where flat detector packs are arranged in
an approximately cylindrical arrangement, illustrates another strength of the
software design of MCViNE. MCViNE takes advantage of the hierarchical rep-
resentation for neutron scatterers, only in this case the elemental homogeneous
305 neutron scatterer is the ^3He detector tube that intercepts neutrons and records

them. MCViNE reuses the code for ray tracing in a composite scatterer for
simulating ^3He detector systems, and the new code needed is a scattering kernel
for the ^3He material that takes into account gas absorption. The ray tracing
through a cylinder takes care of the parallax effect of the detector tube. When
310 a neutron is sent to a detector system shown in Figure 1(c), for example, the
generic ray tracing algorithm for composite scatterers first checks whether the
top level composite scatterer is penetrated by the neutron. If so, all constituents
of the composite scatterer, i.e. the detector packs, are examined to determine
which of them intercepts the neutron. Unless a neutron traverses a gap be-
315 tween detector packs, the detector pack is identified and then its constituents,
the 8 detector tubes, are examined for neutron detection. The path of a neu-
tron through the detector tube is then computed by ray tracing of the neutron
through a cylinder, and a MC sampling picks a point in the path for the neutron
to be absorbed. The position in the tube is used to calculate a unique pixel iden-
320 tifier known as the Pixel ID, according to the scheme readable by the Mantid
software framework [58, 59]. Additionally, the appropriate weighting multiplier
for neutron probability (computed from absorption probability depending on
the ^3He pressure and the length of the neutron path through the tube) and the
time-of-flight are computed for the neutron to be recorded as a detector event in
325 a “virtual detector electronics device”. Our hierarchical approach to detectors
allows for the addition of more details, including details of the charge cloud and
the wire if deemed necessary.

3. Examples

This section presents examples of MCViNE simulations performed for ex-
330 periments on the ARCS, SEQUOIA, and HYSPEC instruments at SNS. These
simulations were performed on one of the SNS data analysis clusters. A typical
analysis cluster has 64 Intel or AMD CPU cores at $\sim 3\text{GHz}$, and simulations
usually run in parallel using 10 cores. Every simulation consists of 4 steps:

Beam simulation. The incident beams on the sample for ARCS, SE-

335 QUOIA, and HYSPEC instruments were simulated. The MCViNE simulation
models were derived from the McStas[12] instrument definitions used in the de-
sign phase of the instruments[45, 48, 60, 61]. In this work, 10^9 neutron events
emitted from the moderator were included in all the simulations, and the neu-
trons at the sample position were saved and reused in the next step. A typical
340 parallel run took about one hour.

Sample scattering. The neutron packets saved in the previous step were
sent to a SampleAssembly component. Typically 10^8 neutron packets were
simulated in a run for any powder sample presented in this section, and it took
minutes to hours to finish, depending on the complexity of the sample assembly.
345 The scattered neutrons were then saved.

Detector interception. Each neutron scattered by the sample was pro-
cessed by a DetectorSystem component and an event was recorded in an event-
mode NeXus file if it intercepted a detector tube. In ray-tracing through a
detector system, the detector tube in which the event was detected was lo-
350 cated using a hierarchical set of detector tubes as described previously, while
the exact location and time-of-flight were determined by a MC selection. The
running time of this step depends on the number of neutrons hitting the detec-
tors, which in turn depends on the number of neutron packets simulated in the
previous step, as well as the user choice of multiple-scattering. Typically, 10^8
355 neutron packets took half an hour.

Reduction. The NeXus data generated in the previous step were reduced
using Mantid[58, 59]. The only difference between the simulated and measured
data is that the intensities in the simulations are computed as the sum of the
probabilities of all packets arriving in the bin of interest, while those in the data
360 are total event counts. The data reduction workflow is therefore identical, and
uses the same code base for both the simulated and the measured data. This
step typically took 10s of minutes to finish for a powder measurement.

The goal of this four-step simulation process was to reproduce the experiment
(including data reduction) by a simulation of high fidelity.

365 This 4-step simulation workflow produces output files such as the simu-

lated scattered neutrons, the simulated event-mode NeXus file, and the reduced $I(Q, E)$ file.

The simulation examples here make use of the following scattering kernels that are described briefly in the Supplemental Material:

- 370 • incoherent elastic scattering
- coherent elastic scattering from powder sample
- incoherent inelastic single-phonon scattering
- coherent inelastic single-phonon scattering from a powder sample
- multi-phonon scattering
- 375 • scattering from a dispersion surface where the dispersion relation and
 the dynamical structure factor are described by analytical functions of
 momentum transfer vector $\mathbf{Q}$

Three examples are presented in the following subsections, two modeling vibrational excitations, and one modeling magnetic excitations. The simplest
380 sample, a vanadium plate, is presented first in Subsection 3.1, where only incoherent scattering kernels are used. Coherent phonon scattering kernels for powder samples are introduced for an aluminum sample in Subsection 3.2. Both Subsection 3.1 and 3.2 demonstrate the ability to easily turn on and off different scattering mechanisms, allowing researchers to gain a better understanding of
385 their contributions. Subsection 3.3 presents a simulation of a measurement on a single-crystal $\text{K}_2\text{V}_3\text{O}_8$ sample, for which a dispersion-surface scattering kernel is used.

In addition to these three examples, MCViNE simulations of Uranium Nitride (UN) measurements performed on the ARCS and SEQUOIA instruments
390 provide an excellent example of the capabilities presented here [9]. In this case, the UN sample exhibited particularly strong multiple scattering due to its size. MCViNE simulations were able to reproduce well the multiple scattering, identified weak scattering from acoustic phonons, and showed that the binary solid

model is a good explanation of the temperature-dependent broadening of the
395 modes of the quantum harmonic oscillator [9].

3.1. Vanadium

Here we present experimental and simulated inelastic spectra for a $50\text{ mm} \times 50\text{ mm} \times 1.2\text{ mm}$ vanadium plate sample in the ARCS instrument. A quick calculation using the total scattering cross section for V shows that such a sample is a 6% scatterer.
400 Vanadium, being the regular calibration standard in neutron scattering experiments, was chosen as the first example for its simplicity (incoherent scattering cross section is much larger than that of coherent scattering, and hence the scattering is isotropic). In the experiment, the sample was approximately perpendicular to the beam, and the incident energy was tuned to 117 meV using a
405 Fermi chopper with 1.5 mm slit spacing and 550 mm radius of curvature, rotating at 600 Hz. In the simulation, the instrument parameters used matched the experimental ones. The simulation sample assembly contains only one homogeneous scatterer for the vanadium plate, which was tilted 96.6 degrees from the beam direction. Different scattering kernels were used for different simulations,
410 but one incoherent elastic kernel and one single-phonon incoherent inelastic kernel were included for all. Incoherent scattering cross section of 5.08 barns and absorption cross section of 5.08 barns [62] were used. All phonon-related scattering kernels use the phonon density of states (DOS) calculated from a Born-von Karman (BvK) model [63], which used force constants originally re-
415 ported in Ref. [64], and tabulated in the Landolt Bornstein series of material properties [65]. Only one universal scale factor was applied to the intensities of all simulated spectra to match the experimental data.

Shown in Figure 4 are $I(Q, \omega)$ plots. The top panel is the experimental result. Panel (b) was simulated without either multi-phonon scattering or multiple-
420 scattering. Panel (c) was simulated with multi-phonon scattering but multiple-scattering was turned off. Comparing (b) and (c), we can see how multi-phonon scattering contributes to intensities at high Q ($> \sim 10\text{ \AA}^{-1}$), especially noticeable at high energy transfer above the single-phonon cut-off energy of $\sim 35\text{ meV}$.

Figure 4: $I(Q, \omega)$ plots of vanadium inelastic spectra obtained from experiment and simulations for a vanadium plate at room temperature in the ARCS instrument. (a) Experiment (b) Simulation without a multi-phonon kernel. Multiple scattering was turned off. (c) Simulation with a multi-phonon kernel. Multiple scattering was turned off. (d) Simulation with a multi-phonon kernel. Multiple scattering was turned on.

Figure 5: Energy spectra integrated over Q range (8,12) inverse angstrom, obtained from experiment and simulations for a vanadium plate placed in the ARCS beam. The intensity axis is in log scale. (a)-(d) same as Figure 4

Panel (d) was done with both multi-phonon and multiple-scattering contribu-
 425 tions. Comparing (c) and (d) shows how the effects of the multiple scattering are
 small but observable, particularly at low Q values ($< \sim 2 \text{ \AA}^{-1}$). As the plate is
 only a 6% scatter, one would expect the multiple scattering to be less than 0.4%,
 consistent with the observation. It also shows that there is less Q -dependence in
 multiple-scattering than in multi-phonon scattering. Figure 5 shows the energy
 430 spectra integrated over momentum transfer range of 8 to $12 \text{ \AA}^{-1}$ in log scale.
 Similarly, we found that multi-phonon scattering contributes more substantially
 than multiple scattering in this Q range.

To examine the agreement between the simulated and the experimental spectra,
 constant momentum cuts and constant energy cuts of the experimental data
 435 (Figure 4(a)) and the simulated data with the most complete collection of scat-
 tering kernels (Figure 4(d)) are presented in Figure 6 and Figure 7, respectively.
 The simulated data in general agree very well with the experimental data, across
 the measured dynamic range and the intensity range, showing features such as
 the asymmetric line shape of the elastic peaks, the detailed balance, and the Q -
 440 dependent phonon-induced energy-loss profiles in the constant-momentum cuts,

Figure 6: Constant momentum cuts of spectra as shown in Figure 4 at different Q values: (a) 8 and (b) 11 $\text{\AA}^{-1}$. The experimental cuts were taken from Figure 4(a), while the simulated cuts were taken from the best simulation incorporating all scattering kernels and multiple-scattering, Figure 4(d). The spectra show decreasing intensities in elastic peaks and increasing relative strength of inelastic scattering on both sides of the elastic peaks, with larger momentum transfers. The deviations of the simulated data from the experimental data ($\Delta I = I_{\text{exp}} - I_{\text{sim}}$, similar thereafter) shown in the lower panels are small and are within error bars. The slightly larger deviations around elastic peaks may be attributed to slight mismatch in determination of elastic lines, the fact that the coherent scattering is neglected in the simulations, as well as uncertainties in moderator profile, and in guide and chopper simulations.

Figure 7: Constant energy cuts of spectra as shown in Figure 4 at different E values: (a) -20 (b) 0 (c) 20 and (d) 40 meV. The experimental cuts were taken from Figure 4(a), while the simulated cuts were taken from the best simulation incorporating all scattering kernels and multiple-scattering, Figure 4(d). The elastic scattering in (b) weakens with higher Q due to the Debye-Waller factor; the inelastic scattering in other panels strengthens with higher Q : for panels (a) and (c), this trend is dominated by the one-phonon scattering proportional to the Q^2 factor in addition to the same Debye-Waller factor, while for panel (d) for which the energy transfer of 40 meV is beyond the single-phonon energy cut-off, it is dominated by the two-phonon scattering proportional to the Q^4 factor. The dip shown in every panel is typical of the plate sample geometry and a result of absorption along the sample width (the dark angle). The deviations of the simulated data from the experimental one (shown in the lower panels) are in general smaller than error bars. The peaks in the deviation curve at the lower panel of (b) are beyond error bars, but they match positions of powder diffraction peaks as indicated by the vertical dotted lines, and most likely can be accounted for by the fact that the coherent scattering from V are neglected in the simulations.

and the dark-angle dips in the constant-energy cuts. Also in the constant energy cuts (Figure 7), spikes in intensities (e.g., at $E = -20$ meV, $Q \sim 10 \text{ \AA}^{-1}$, and at $E = 20$ meV, $Q \sim 9 \text{ \AA}^{-1}$) result from insufficient filling of the displayed Q, ω histogram bins by the detector pixels. While additional analysis may be
445 able to correct for this effect, it is instructive that the detailed modeling of the ARCS detector array almost exactly matches the measured data, while typical MC simulations would miss this effect due to simplified detector models.

The uncertainties of this simulation arise from the following factors: deviation of the simulated incident beam from the actual neutron beam at the ARCS
450 instrument; differences between the sample shape specification in simulation and the actual sample shape, such as its dimensions, and its orientation relative to the incident beam; the uncertainties in the physical and geometrical properties of the detector packs in the detector system, especially their positions and orientations; the deviation of the sample temperature in simulation from
455 the actual temperature; and the uncertainties in the sample material such as impurities and contamination, neglect of Bragg reflections in simulations, and uncertainties in the phonon density of states (DOS) of vanadium.

The simulation of the incident beam is in part validated by comparison to the first beam monitor, and scattering from 2,5-diiodothiophene ($\text{C}_4\text{H}_2\text{I}_2\text{S}$) [47].
460 This partial validation is corroborated by the agreement observed in the elastic peaks of $I(E)$ spectra (Figure 6). The sample dimensions and its position and orientation influence the position of the elastic peaks, and the position and the width of the dark angle, which all show excellent agreement between experimental and simulated data. Uncertainties in positions and orientations of the
465 detector packs can result in incorrect mapping from pixels to Q, E coordinates. The fact that the simulated data show the same artifacts at the low-pixel-count detector area as the experimental data indicates that these errors are minimal. The deviation of experimental sample temperature from the simulation value is not expected to be larger than 10 Kelvin, which is consistent with excellent
470 match in detailed balance between the simulation and the experiment shown in Figure 6. An examination of Figure 7(b) shows a series of sharp peaks, which

Figure 8: Experimental and best-simulated energy spectra obtained by integrating over Q range (8,12) inverse angstrom of the spectra as shown in Figure 4 (a) and (d). The intensity scale is expanded to highlight the inelastic spectra.

arises from the Bragg reflections in the sample that were not included in the simulations. These may account for some differences in the elastic peaks in Figure 6 as well. The excellent agreement in all the other cuts of Figure 7 shows
 475 this does not affect the spectroscopic results. The remaining factor is the uncertainties in the phonon DOS, which is the main source of uncertainties in this simulation.

The discrepancy between the simulated data and the experimental data, relevant to researchers interested in phonons, is easier to observe from Figure 8.
 480 The double peaks near 20 and 28 meV both appear to shift to the right in the experimental data, compared to the simulated one. This discrepancy has its origin in the phonon DOS used in the simulation, which is computed from a BvK model fitted to an X-ray determination of phonon dispersions[64]. Consistent with the discrepancies observed here, this BvK model slightly underestimated
 485 phonon energies when compared to a phonon DOS spectrum measured using inelastic neutron scattering (see Figure 10 of [64]). Actually, the uncertainty of measured vanadium phonon DOS reported over the years is larger than the discrepancy observed here (see, for example, Figure 2 of [66]).

3.2. Aluminum

490 In this example, we present experimental and simulated inelastic spectra from a 60 mm×60 mm×4 mm polycrystalline aluminum (1100 alloy) plate in the ARCS instrument. A quick calculation using the total scattering cross section for Al shows that such a sample is a 5% scatterer. In the experiment, the sample was placed approximately at 135 degrees from the beam, and the incident energy
495 was tuned to 80.5 meV using the same Fermi chopper slit package as used in the previous example for vanadium, spinning at 480 Hz. In the simulation, the instrument parameters used matched the experimental ones. The simulation sample assembly contains only one homogeneous scatterer for the aluminum plate. Different simulations made use of different combinations of scattering
500 kernels. Tabulated Al cross sections [62] were used. All phonon-related scattering kernels use phonon energies and polarization vectors computed on a regular grid in a Brillouin zone from a BvK model [67]. The broadening of the phonon modes was not included. Only one universal scale factor was applied to all simulated spectra to match the experimental data.

505 Figure 9 shows $I(Q, \omega)$ plots for the aluminum plate. The experimental result is given in panel (a) and panels (b)-(e) show simulated data. In (b) only the incoherent elastic and incoherent single phonon scattering are included. In this plot the maximum intensity for the color scale is reduced by the ratio of incoherent/coherent cross sections of aluminum, so one can see the details in the
510 plot. The numerical values on the colorbar give an indication of the scaling. In (c) only the coherent elastic (powder diffraction) and the coherent single-phonon inelastic scattering are included. In (d), all of the kernels in (b) and (c) with the addition of a multi-phonon kernel using the incoherent approximation. In (e), all of the kernels in (d) are used with multiple scattering turned on. Overall the
515 features shown in the experimental data (a) and the simulated data (e) agree very well. Comparison of (b) and (c) shows that coherent scattering gives rise to more features such as diffraction peaks and phonon dispersion curves. It is evident from comparing (c) and (d) that multiphonon scattering increases in intensity at higher Q . The most obvious difference in (d) and (e) is in the elastic

Figure 9: $I(Q, \omega)$ plots of aluminum inelastic spectra obtained from experiment (a) and simulations (b)-(e) of an aluminum plate at room temperature in the ARCS instrument. Scattering kernels included in the simulations are (b) incoherent elastic and incoherent inelastic single-phonon scattering (see note on intensity scaling in text), (c) coherent elastic (powder diffraction) and coherent inelastic single-phonon scattering, (d) all kernels included in (b) and (c) plus a multi-phonon kernel using an incoherent approximation and (e) all kernels included in (d) plus multiple scattering.

Figure 10: Energy spectra integrated over Q range (6,10) inverse angstrom, obtained from experiment and simulations for an aluminum plate placed in the ARCS beam. The intensity axis is in log scale. (a)-(e) same as Figure 9

line, which shows that multiple scattering of coherent elastic scattering seems to contribute similarly to incoherent scattering in the elastic line. The elastic lines in (a) and (e) seem to show that the sample used in the experiment may contain traces of an additional phase, most likely from a surface layer of Al_2O_3 . Figure 10 shows energy spectra integrated over a range of momentum transfer from 6 to 10 $\text{\AA}^{-1}$ in log scale. Similar to the vanadium measurement, we found that multi-phonon scattering plays a significant role in the observed intensity, whereas multiple scattering plays little role in this Q range. This is expected as the sample is only a 5% scatterer.

Similar to the vanadium study in the previous section, we further examine the agreement between the simulated and the experimental spectra by taking constant momentum cuts and constant energy cuts of the experimental data (Figure 9(a)) and the simulated data with the most complete collection of scattering kernels (Figure 9(e)). These cuts are presented in Figure 11 and Figure 12, and they again display strong agreement between the experimental and simulated data. For Figure 11, the maximum deviations occur near the elastic peak. Similarly, the biggest differences in Figure 12 are observed for the elas-

Figure 11: Constant momentum cuts of spectra as shown in Figure 9 at different Q values: (a) 3 (b) 5 (c) 7 and (d) $9 \text{ \AA}^{-1}$. The experimental cuts were taken from Figure 9(a), while the simulated cuts were taken from the best simulation incorporating all scattering kernels and multiple-scattering, Figure 9(e). The deviations of the simulated data from the experimental data are plotted in the lower panels. The main contribution to the larger deviations around the elastic peaks most likely comes from the texture in the sample.

Figure 12: Constant energy cuts of spectra as shown in Figure 9 at different E values: (a) -20 (b) 0 (c) 20 and (d) 40 meV. The experimental cuts were taken from Figure 9(a), while the simulated cuts were taken from the best simulation incorporating all scattering kernels and multiple-scattering, Figure 9(e). The deviations of the simulated data from the experimental one (shown in the lower panels) in general are smaller than the error bars. The discrepancies in (b) are from differences in the measured and calculated Bragg peak intensities. These arise from the fact that the sample is not a perfect powder.

tic scattering in (b). These indicate that the measured Bragg peak intensities vary from the model: an isotropic powder average for Al. This could arise from texture, preferred grain orientation, or incomplete sampling of the powder[68].

540 The uncertainties of this simulation, like the case of vanadium, arise mainly from the uncertainties in the phonon data, which is the major input to all phonon-related kernels used in the simulation, only in this case the phonon data is not just a simple DOS curve. This phonon data input, existing in the form of energies and polarization vectors of all phonon branches, was computed for all points on a regular grid inside the first Brillouin zone, from a
545 BvK model fit to phonon dispersions measured along the [100], [110], and [111] directions[67]. Small changes in the force constants in the BvK model can result in large fluctuations of the computed phonon energies and polarizations. Hence, the discrepancy between the experimental data (Figure 10(a)) and the
550 simulated data (with all kernels, Figure 10(e)) was not unexpected. Another possible contributing factor is the fact that the broadening of Al phonon modes [69, 70] was not taken into account in our simulation.

3.3. $K_2V_3O_8$ single crystal

We now present experimental and simulated inelastic single-crystal spectra
555 for a $K_2V_3O_8$ sample [71] measured at the HYSPEC instrument [51], a hybrid spectrometer at SNS with a focusing monochromator and a movable detector vessel. The sample consisted of 5 co-aligned crystals with an overall cylindrical shape approximately 3.8 cm in diameter and 2.5 cm in height. The sample was oriented so that at zero degrees of rotation angle its [100] direction was along
560 the beam and its [001] direction pointed upward vertically. Measurements were performed at 1.5 K with an incident energy of ~ 7 meV with a Fermi chopper frequency of 180 Hz. The detector vessel was oriented so that neutrons scattered from the sample in the horizontal plane were measured in the scattered angle range of -75 to -15 degrees. To span reciprocal space, the goniometer angle was
565 swept from 40 to -50 degrees in 0.5 degree steps and then from -50 to -28 degrees in 1 degree steps.

The simulation was done for a scan matching the experimental setup. The sample assembly contains one homogeneous scatterer for the $\text{K}_2\text{V}_3\text{O}_8$ sample with a shape matching the overall shape of the sample in the experiment. Two
570 scattering kernels were included in the simulation: one incoherent elastic scattering kernel to approximate the elastic line, and one dispersion-surface scattering kernel for simulating the scattering from the spin-wave.

In $\text{K}_2\text{V}_3\text{O}_8$ the long-wavelength spin-wave dispersion is well described by a result for the quantum ($S=1/2$) square lattice Heisenberg antiferromagnet:

$$E(\mathbf{Q}) = 2\tilde{J}\sqrt{1 - \gamma_{\mathbf{Q}_{//}}^2} \quad (1)$$

575 with the dynamic structure factor

$$S(\mathbf{Q}, E) = \frac{1 - \gamma_{\mathbf{Q}_{//}}}{2\sqrt{1 - \gamma_{\mathbf{Q}_{//}}^2}} \delta(E - E(\mathbf{Q})) \quad (2)$$

where $\gamma_{\mathbf{Q}_{//}} = \cos(h\pi) \cos(k\pi)$, $2\tilde{J} = 2.563$ [71]. The differential cross section is

$$\left(\frac{d^2\sigma}{d\Omega dE_f} \right) \sim \frac{k_f}{k_i} |F(Q)|^2 [n(E) + 1] (1 + \cos^2 \phi) S(\mathbf{Q}, E) \quad (3)$$

where k_i and k_f are the magnitudes of the incident and final neutron wave vectors, $F(Q)$ is the magnetic form factor for V^{4+} [72], $n(E) + 1$ is the Bose occupation factor, and $1 + \cos^2 \phi$ is a polarization term (ϕ is the angle between
580 $\mathbf{Q}$ and the easy c-axis).

In the treatment of both experimental and simulated data, Mantid was used to reduce the measured NeXus file to NXSPE format, a specialized intermediate inelastic neutron data format, at each goniometer angle, and then a Python program was used to project data in NXSPE files to the four dimensional $\mathbf{Q}$, E
585 space. Slices along desired $\mathbf{Q}$ directions could then be taken.

Shown in Figure 13 are experimental and simulated slices along axes of $\mathbf{Q} = [h10]$ and energy. The spin wave dispersion in the energy range between ~ 0.3 and ~ 2.1 meV shows good agreement between experimental and simulated data. In the experimental data, the noise in the energy range of $[0.25, 0.7]$ is
590 higher than the noise at higher energies. This is due to elastic scattering from

Figure 13: Slices along the $\mathbf{Q}=[h10]$ axis and the energy axis from (a) experiment and (b) simulation, taken in the range $l=(-0.3, 0.3)$ and $k=(0.93, 1.07)$.

Figure 14: Constant energy cuts of the slices as shown in Figure 13 in the energy range of [1.2, 1.3] meV. A background term and a scaling factor were the only parameters used to fit the simulated data to experimental data. The goodness of fit, reduced χ^2 , was 2.56.

the cryostat, which was subtracted from the data. Both plots show a distinctive feature – for the dispersion near $[010]$ the right branch is sharper than the left branch, while the dispersion branches near $[210]$ are largely symmetric in their broadening. This effect is more clear in Figure 14, where constant-energy
595 cuts over $[1.2, 1.3]$ meV are plotted against $\mathbf{Q} = [h10]$ for the experimental (circles with error bars) and the simulated (solid line) intensities. Both the experimental data and simulated data show that the peak near $h = 0.15$ is much sharper than that near $h = -0.15$. Such an effect is expected due to different focusing conditions of the resolution ellipsoid [73, 74]. The spin-wave
600 dispersion above ~ 2.1 meV ($h \sim 0.33$, for example) has weaker intensity in the experimental data than expected from the simulated data, which could be attributed to mode splitting near the zone boundary [71].

4. Conclusions

The MCViNE software package for Monte Carlo neutron ray tracing sim-
605 ulations is based on modern object-oriented software design that decomposes neutron scatterers into a hierarchy of composite and elemental scatterers. This software design elegantly solves algorithmic problems including multiple scattering in a sample assembly, and ray tracing in a sophisticated detector system. Multiple scattering and instrument resolution are included naturally in
610 MCViNE simulations, and simulation of ray-tracing in a complex detector system such as those of the ARCS and SEQUOIA instruments is straightforward. Adding, removing, and modifying scattering kernels in the simulations can help show the contributions of different types of scattering events to the experimental data. The examples of scattering from vibrational and magnetic excitations
615 presented here and elsewhere[9] demonstrate that such simulations can improve our understanding of the underlying physics of neutron spectra.

Limitations of the MCViNE software package include (1) the complexity of sample assembly or detector system can be limited by available computing resources (memory and computation time); (2) it currently only supports ho-

620 homogeneous scatterers, and this means materials with non-uniform distribution
of defects, for example, can not be simulated without approximations; (3) it
has a limited but expandable library of scattering kernels. For example, for
magnetic systems, it currently only supports spin-wave dispersions that can be
expressed as analytical functions; (4) MCViNE currently relies on components
625 adapted from other MC ray tracing packages to handle many neutron optical
components such as guides and choppers, and thereby inherits their limitations.

MCViNE is freely available for the Linux platform. More details about the
conditions of use and license can be found at <http://danse.us/trac/MCViNE/wiki/license>.
Details on build and installation, usage, source repository, and user support of
630 MCViNE are available in the documentation [32]. Feedback to the MCViNE de-
velopers can be provided through the MCViNE user mailing list [http://groups.google.com/group/mcvin-](http://groups.google.com/group/mcvin-users)
[users](http://groups.google.com/group/mcvin-users).

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