Adsorption and Diffusion of Atomic Oxygen and Sulfur at Pristine and Doped Ni Surfaces with Implications for Stress Corrosion Cracking

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ABSTRACT. A density-functional-theory modeling study of atomic oxygen/sulfur adsorption and diffusion at pristine and doped Ni(111) and (110) surfaces is presented. We find that oxygen and sulfur feature comparable adsorption energies over the same surface sites, however, the surface diffusion of sulfur is characterized by an activation barrier about one half that of oxygen. Calculations with different alloying elements at Ni surfaces show that Cr strongly enhances surface binding of both species in comparison to Al. These results in combination with previous modeling studies help explain the observed differences in selective grain boundary oxidation mechanisms of Ni-Cr and Ni-Al alloys.

KEYWORDS. Density Functional Theory; Diffusion; Ni Alloys; Oxidation; Sulfidation; Corrosion.

Introduction.

Nickel-base alloys represent an important class of structural materials for advanced energy systems due to their ability to withstand a range of aggressive temperatures, pressures and mechanical loadings [1-3]. Nevertheless, these corrosion-resistant metallic alloys can be susceptible to localized attack and cracking leading to component failure. One of the most common degradation modes is due to selective oxidation processes at grain boundaries that lead to intergranular (IG) corrosion, crack initiation and propagation [4-8].

Recent advanced characterization techniques have provided new insights into selective grain-boundary oxidation reactions driving IG corrosion and stress corrosion cracking (SCC) of alloys [9-16]. For example, analytical transmission electron microscopy (ATEM) and atom probe tomography (APT) investigations [17,18] demonstrated the formation of isolated discrete oxide precipitates (NiAl_2O_4) along grain boundaries of Ni-4Al alloys after exposure to 360°C hydrogenated water, consistent with oxygen ingress through the metal matrix and classical internal oxidation. On the other hand, grain boundaries of Ni-5Cr alloys exposed to identical high-temperature water conditions exhibit the formation of a continuous IG Cr-rich oxide inconsistent with internal oxidation. These differences can be attributed to the different diffusion behavior of Al versus Cr, where more facile Cr diffusion to oxidation fronts in grain boundaries results in a rapid consumption of oxygen, whereas slower Al diffusion allows oxygen ingress and internal oxidation to occur. Our recent first-principles modeling results [19] on the vacancy-mediated diffusion of various alloying metal elements in the bulk and along grain boundaries of Ni showed a faster Cr diffusion as compared to Al, especially along the high-energy grain boundaries, thus generally supporting this hypothesis.

Key differences were observed when comparing IG attack of commercial Ni-Cr-Fe alloys (alloy 600) during exposure to high-temperature hydrogenated water with and without surface contamination of sulfur [20,21]. Solid-state grain boundary ingress of sulfur and internal sulfidation was observed when sulfur was present, while oxygen ingress and internal oxidation in the metal grain boundary was not detected in either case. The oxidation/sulfidation behavior documented for this Ni-Cr alloy in hydrogenated water was very similar to that found in higher temperature gaseous environments [22,23] where sulfur was discovered to first diffuse into grain boundaries forming Cr sulfides followed by oxidation reactions that release sulfur deeper into the material. Contrasting the results obtained for oxygen and sulfur cases is not only important for the general understanding of fundamental differences in solid-state electrochemistry of Ni-base alloys, but also because sulfur is a common contaminant in many service environments and an impurity in alloys [24-26]. In order to better understand the

observed differences in grain boundary oxidation/sulfidation behavior of various Ni-base alloys, it is also important to examine how oxygen and sulfur atoms interact with both pristine and Ni surfaces doped with common alloying elements, an aspect that will be addressed in this study.

Despite a large body of previous experimental information about interfacial oxidation processes promoting SCC in Ni-base alloys, detailed microscopic understanding is still lacking. The inherent complexity of the corrosion/oxidation behavior of Ni-base alloys has triggered a number of computational atomistic studies aimed to elucidate the mechanisms and kinetics of electrochemical reactions, adsorption behavior and species diffusion in the bulk and at interfaces [19,27-33]. Since many degradation processes occur in aqueous environments, first-principles studies have been devoted to understanding of the interactions between water and Ni surfaces [30,31]. These investigations resulted in a better atomic picture of H₂O adsorption at various sites on Ni surfaces, reaction mechanisms of H₂O dissociation and the associated energy barriers. Interactions between atomic oxygen and particularly sulfur with the Ni surface are still poorly understood. Furthermore, because alloying elements can drastically change the bulk and interfacial properties of Ni, it is crucial to understand how different elements interact with the adsorbed species. Despite general similarities between oxygen and sulfur, recent experimental studies have clearly demonstrated significant differences in their effects on Ni-base alloys [20,21]. Therefore, to develop a better model of early stages of oxidation and sulfidation, it is instructive to contrast the adsorption and diffusion behaviors of oxygen and sulfur and understand how the nature of alloying elements in Ni metal affects interfacial and surface properties. Since the high-energy grain boundaries play a dominant role in oxidation and corrosion behavior of Ni-base alloys, the approach in this paper is to model adsorption reactions and species transport at the Ni surfaces that are characterized by similar open structures. This also allows us to systematically compare the effect of various alloying elements without possible complications arising from atomic reconstructions of the high-energy grain boundaries associated with the presence of alloying and adsorbed species.

Computational Details.

Density-functional-theory (DFT) calculations were performed using the VASP code [34,35] within the Perdew-Burke-Ernzerhof (PBE) parametrization of the generalized gradient approximation (GGA) [36] combined with the projector augmented wave (PAW) potentials [37]. All calculations were carried out spin-polarized with a plane wave cutoff energy of 400 eV. The Ni(111) surface was modeled as a slab consisting of five Ni layers with 4×4 expansion of the surface cell resulting in a distance of 9.955 Å between periodic images of adsorbed atomic species. The Ni(110) surface was modeled as a slab with seven Ni layers and 4×2 surface periodicity with the dimensions of 7.039 Å × 9.955 Å. A vacuum gap of at least 10 Å was used to minimize interaction between surfaces of adjacent slabs. During geometry optimization only the middle Ni layer and the lattice constant were fixed. A lattice constant of 3.5196 Å found from the Ni bulk geometry optimization was used in the study. Optimization of atomic positions was performed until all atomic forces were less than 0.02 eV/Å and the total energy was converged to better than 10⁻⁶ eV. The Brillouin zone integration was done using a 3×3×1 Monkhorst-Pack mesh, whereas the use of a 5×5×1 grid showed only marginal changes in both Ni surface energies and species adsorption energies. To calculate activation energy barriers for species diffusion at the surfaces, we employed the climbing image nudged elastic band (CI-NEB) method [38]. Species adsorption energies were calculated as $E_{ads} = E_{surf+adsorbate} - E_{surf} - E_{adsorbate}$, where $E_{surf+adsorbate}$ and E_{surf} are the energies of the surface with and without an adsorbed species (atomic oxygen or sulfur), respectively, and $E_{adsorbate}$ is the energy of an oxygen or sulfur atom in a 15×15×15 Å³ box. This definition implies negative adsorption energies for energetically favorable adsorption processes.

Results and Discussion

The first step was to consider the adsorption energetics for oxygen and sulfur atomic species over various adsorption sites at the pristine and doped (111) and (110) surfaces of Ni that are known to be the most stable Ni facets. Figures 1 and 2 show different adsorption sites at the Ni(111) and (110) surfaces, while Tables 1 and 2 list the corresponding calculated energies for the adsorption of oxygen and sulfur atomic species at the pristine Ni surfaces. It is seen that at the Ni(111) surface the hollow-fcc position is the most energetically favorable for both oxygen and sulfur adsorption; this site is slightly more preferable than the hollow-hcp site while the top site is the least favorable. We observe the same trend for the Ni(110) surface, however, sulfur adsorbs to this surface a little stronger than oxygen on all sites examined. For the Ni(110) surface we also considered another hollow adsorption site which is near the bridge-long site but moved left into the midst of the triangle (see Figure 2). However, during

optimization both oxygen and sulfur atomic species converged to the bridge-long position. It is also apparent that the most stable adsorption configurations for both (111) and (110) surfaces are overall quite comparable in energy (-5.87 versus -5.61 eV) for the most favorable adsorption sites, see Tables 1 and 2). In addition, a step was created on the Ni(111) surface by removing half of the uppermost surface Ni atoms. The calculated adsorption energies turned out to be very similar to those obtained for the hollow site at the Ni(110) surface, being slightly higher for the step on the Ni(111) surface for both oxygen and sulfur due to the appearance of unsaturated Ni bonds.

Figure 1. Side (left) and top (right) view of the Ni(111) surface supercell with the corresponding surface adsorption sites. Only half of the slab is shown on the left figure. Color coding helps distinguish different Ni planes.

Figure 2. Side (left) and top (right) view of the Ni(110) surface supercell with the corresponding surface adsorption sites. Only half of the slab is shown on the left figure. Color coding helps distinguish different Ni planes.

Figure 3. Energy profiles for oxygen and sulfur diffusing at the pristine Ni(111) surface between two neighboring hollow-fcc adsorption sites. Inset shows the position of a diffusing species at the local energy minimum (hollow-hcp site) halfway between initial and final states.

Figure 4. Energy profiles for oxygen and sulfur diffusing at the pristine Ni(110) surface between the two neighboring hollow adsorption sites.

Tables 3 and 4 illustrate how the energies of oxygen/sulfur adsorption change in the presence of an alloying metal element added to the uppermost surface as the nearest neighbor to the adsorbed species for the Ni(111) surface. First of all, we observe that adsorption energies vary substantially depending on the alloying metal element. Cr and Mn alloying elements feature the most stable adsorption configurations followed by Fe and Al. In these cases, oxygen and sulfur atomic species are expected to preferentially adsorb on the more reactive alloying element rather than on the Ni matrix atoms. This is, however, not the case for Cu, which is relatively noble compared to Ni, where much less stable oxygen/sulfur adsorption is found in comparison to the host Ni atoms. The stronger binding of atomic species is consistent with the calculated Bader charges on the alloying element and oxygen/sulfur exhibiting larger ionicity.

An important related issue regards the mobilities of the alloying elements themselves, relative to the rates of oxygen and sulfur diffusion. Our recent first-principles study [19] of vacancy-mediated diffusion across a wide series of alloying metal elements used in Ni-base alloys demonstrated that Cr and Mn exhibit smaller activation barriers than other metal species considered here, both for the bulk

case and along grain boundaries (hence their emphasis in the present study). High-energy grain boundaries exhibit remarkably lower activation barriers than those calculated for the bulk and therefore such grain boundaries can serve as efficient conduits for a rapid diffusion of minor alloying elements. Combining these results with the finding of much stronger oxygen/sulfur adsorption on the Cr (and Mn) atoms at Ni surfaces, we can suggest that the rate-limiting step of selective grain boundary oxidation is the bulk diffusion of alloying metal elements. When Cr reaches the surface their diffusion should be much more facile along the grain boundaries until they encounter oxygen/sulfur species and form very stable immobile near-surface metal-oxygen or metal-sulfur clusters. These clusters are expected to be precursors for the formation of stable oxide or sulfide precipitates such as Cr_2O_3 or Cr_2S_3 at the grain boundary region. Alloying elements other than Cr and Mn exhibit a substantially smaller preference for oxygen/sulfur adsorption as compared to the host Ni surface atoms. This is particularly true for Cu that is characterized by even smaller oxygen/sulfur adsorption energies than the host Ni atoms, while Al and Fe exhibit generally similar adsorption energies to Ni. Slower diffusion of these alloying metal elements (versus Cr and Mn) in the bulk and along the grain boundaries further limits their supply and together with weaker oxygen/sulfur surface adsorption can enable the ingress of oxygen/sulfur into the bulk matrix. These findings help explain oxygen ingress and internal oxidation in a Ni-Al model alloy [17] and the absence of oxygen ingress and internal oxidation for Ni-Cr alloys [18].

It is further seen that oxygen and sulfur show comparable adsorption energetics across the same adsorption sites on the two Ni surfaces. The most prominent difference is the kinetics of oxygen and sulfur diffusion. While it was calculated that oxygen should diffuse much faster than sulfur in bulk Ni [19], the opposite is found on Ni surfaces. Calculated activation barriers for sulfur surface diffusion are about one half those for oxygen, both on the (111) surface (Figure 3) and on the (110) surface (Figure 4). This suggests that the sulfur supply can be faster than oxygen specifically along high-energy grain boundaries. This finding could partially explain the difference in the observed mechanisms of grain boundary oxidation versus sulfidation in Ni-Cr alloys, where the faster grain boundary diffusion of sulfur as compared to oxygen could enable deeper penetration and internal sulfidation. Conversely, the relatively slow diffusion of oxygen combined with the fast diffusion of Cr and strong Cr-oxygen binding energy prevents solid-state oxygen ingress into the matrix needed for internal oxidation.

Conclusions

DFT-calculations have provided new details on the adsorption and diffusion behavior of oxygen and sulfur on both pristine and doped Ni metal surfaces. Both species prefer adsorption at low-energy

hollow adsorption sites, while sulfur exhibits a significantly lower diffusion barrier than does oxygen. This difference may partially explain the observed tendency of Ni-Cr alloys to exhibit internal sulfidation in environmental conditions that do not allow internal oxidation. Comparing different alloying species has also revealed that Cr and Mn exhibit the strongest binding energies to both oxygen and sulfur, while Al and Fe exhibit binding energies that are relatively similar to that of Ni. Taken together, the results suggest that the relatively slow mobility and weak bonding of Al with O, in comparison to Cr diffusivity and Cr-O binding energies, enables the experimentally observed internal oxidation of Ni-Al alloys that is not found in similarly tested Ni-Cr alloys.

Table 1. Adsorption energies (in eV) for atomic oxygen and sulfur for various adsorption sites (see Figure 1) at the pristine Ni(111) surface.

	Top	Hollow-fcc	Hollow-hcp	Bridge	Step
Oxygen	-4.02	-5.87	-5.76	-5.76	-5.67
Sulfur	-4.06	-5.62	-5.56	-5.36	-5.85

Table 2. Adsorption energies (in eV) for atomic oxygen (O) and sulfur (S) for various adsorption sites (see Figure 2) at the pristine Ni(110) surface.

	Top	Hollow	Bridge-short	Bridge-long
Oxygen	-4.35	-5.61	-5.55	-5.40
Sulfur	-4.99	-5.93	-6.19	-5.48

Table 3. Adsorption energies E_{ads} (in eV) for hollow-fcc and top positions of the adsorbed oxygen atom, as well as metal-oxygen distances $d(\text{M—O})$ (in Å) and atomic charges q for the top configuration over various dopants at the Ni(111) surface.

	E_{ads} (hollow-fcc)	E_{ads} (top)	$d(\text{M—O})$	$q(\text{M})$	$q(\text{O})$
Ni	-5.87	-4.02	1.67	0.27	-0.63
Al	-6.11	-4.22	1.69	1.84	-1.37
Cu	-4.70	-2.34	1.73	0.26	-0.72
Fe	-6.02	-4.43	1.64	0.74	-0.77
Cr	-9.06	-8.67	1.60	1.32	-0.84
Mn	-8.83	-7.73	1.61	0.93	-0.74

Table 4. Adsorption energies E_{ads} (in eV) for hollow-fcc and top positions of the adsorbed sulfur atom, as well as metal-sulfur distances $d(\text{M—S})$ (in Å) and atomic charges q for the top configuration over various dopants at the Ni(111) surface.

	E_{ads} (hollow-fcc)	E_{ads} (top)	$d(\text{M—S})$	$q(\text{M})$	$q(\text{S})$
Ni	-5.62	-4.06	2.01	0.02	-0.46
Al	-6.76	-4.87	1.69	1.63	-0.80
Cu	-5.35	-3.04	2.06	0.12	-0.21
Fe	-5.54	-4.16	2.04	0.48	-0.56
Cr	-8.34	-7.17	2.03	1.03	-0.59
Mn	-8.21	-6.39	2.00	0.68	-0.56

Table 5. Adsorption energies E_{ads} (in eV) for hollow and top positions of the adsorbed oxygen atom, as well as metal-oxygen distances $d(\text{M—O})$ (in Å) and atomic charges q for the top configuration over various dopants at the Ni(110) surface.

	E_{ads} (hollow)	E_{ads} (top)	$d(\text{M—O})$	$q(\text{M})$	$q(\text{O})$
Ni	-5.61	-4.35	1.65	0.37	-0.69
Al	-5.98	-4.59	1.67	2.10	-1.31
Cu	-4.78	-2.76	1.71	0.30	-0.70
Fe	-5.76	-5.08	1.63	0.77	-0.77
Cr	-6.70	-6.48	1.60	1.38	-0.86
Mn	-5.82	-5.27	1.61	1.02	-0.79

Table 6. Adsorption energies E_{ads} (in eV) for hollow and top positions of the adsorbed sulfur atom, as well as metal-sulfur distances $d(\text{M—S})$ (in Å) and atomic charges q for the top configuration over various dopants at the Ni(110) surface.

	E_{ads} (hollow)	E_{ads} (top)	$d(\text{M—S})$	$q(\text{M})$	$q(\text{S})$
Ni	-5.93	-4.99	2.00	0.36	-0.69
Al	-5.61	-3.58	2.12	2.04	-1.04
Cu	-5.49	-2.98	2.04	0.16	-0.52
Fe	-5.83	-4.13	2.02	0.56	-0.61
Cr	-6.07	-4.72	2.02	1.11	-0.66
Mn	-5.86	-3.47	1.99	0.78	-0.62

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